

Modèles hiérarchiques et réduction de modèles (PART I)

Adaptation de bases POD et Hyper Réduction

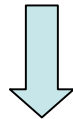


David Ryckelynck
Centre des Matériaux

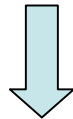
Base modale

Associée à un modèle linéaire sous-jacent

$$M \ddot{q}(t) + D \dot{q}(t) + K q(t) + f_{NL}(q(t), \dot{q}(t)) = f(t)$$



$$M \ddot{q}(t) + K q(t) = \mathbf{0}$$

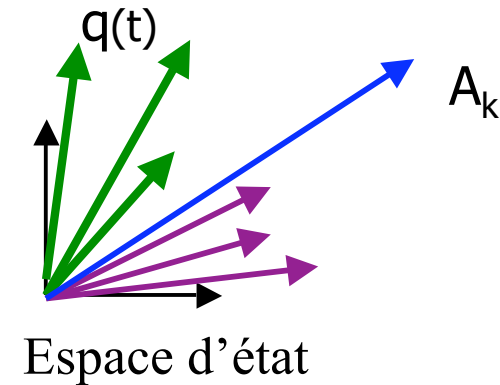


$$q(t) = [\Phi, A_s] \cdot a(t)$$

Base associée à différents états

Base POD

Associée à une suite d'états

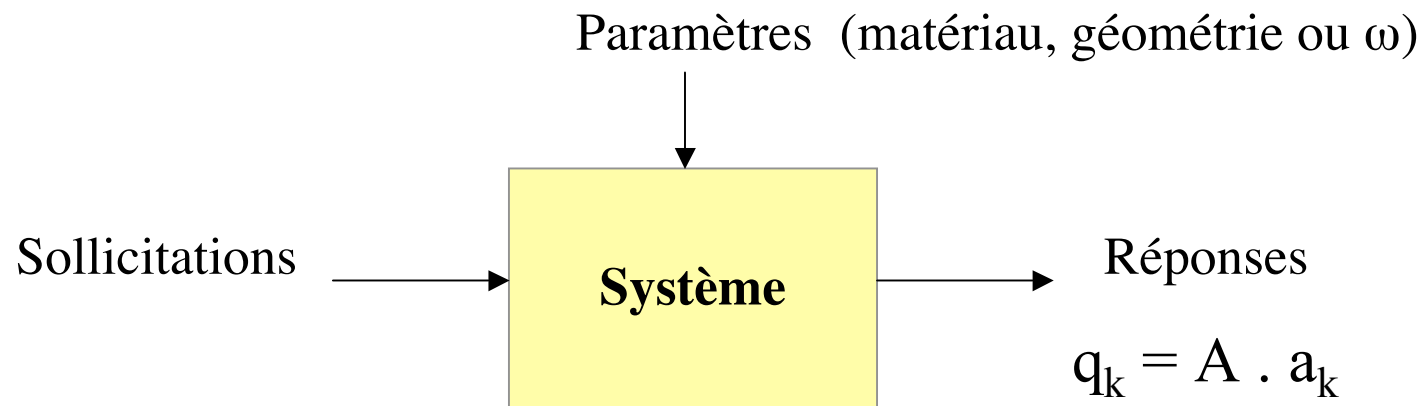


$$q(t) = A \cdot a(t)$$

Modèle d'ordre réduit
Variables d'état réduites : $a(t)$

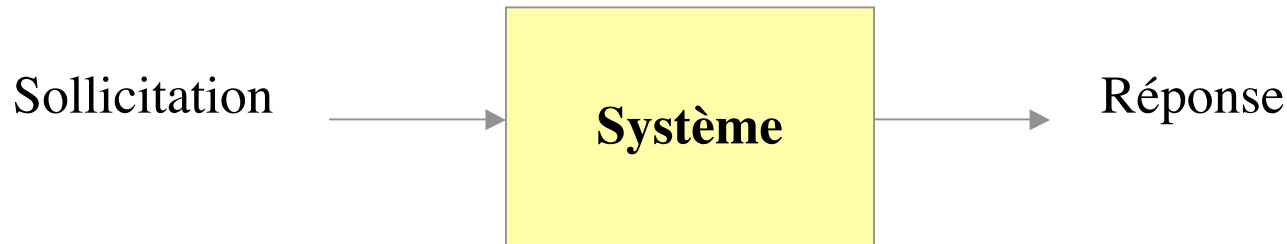
Ce que l'on attend d'une méthode de réduction

Réduire les coûts de calcul d'études paramétriques.

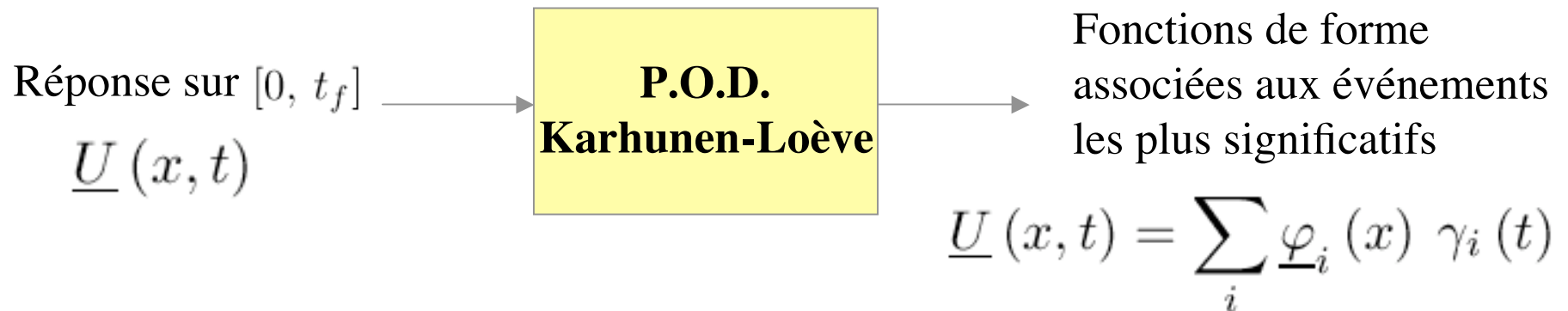


Approches classiques :

- exploiter la linéarité d'un modèle et les caractéristiques des sollicitations
- exploiter l'évolution dans le temps de la réponse du système



Écoulements turbulents : analyse statistique de l'évolution de l'état du système



Lumley 1967 Sirovich 1987 Aubry et co. 1991 Krysl Lall 2001

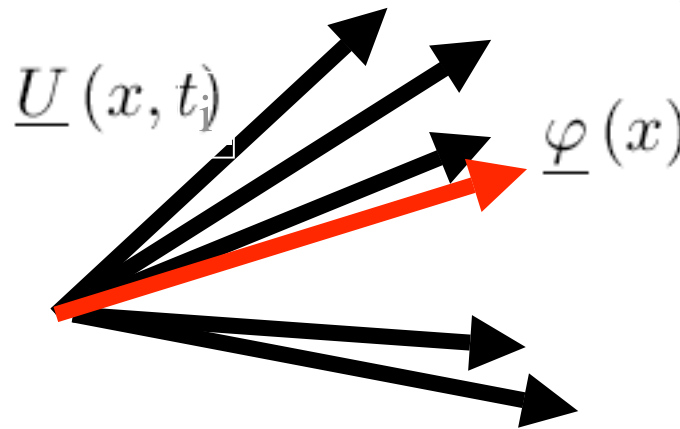
Pas d'adaptation des fonctions de forme du modèle d'ordre réduit

Pas de réduction du nombre de points d'intégration

**Sélection de fonctions de forme à l'aide du développement de
Karhunen-Loève (processus stochastique)
ou de la décomposition orthogonale propre (processus déterministe)**

Sous-espace engendré
par les réponses du
système

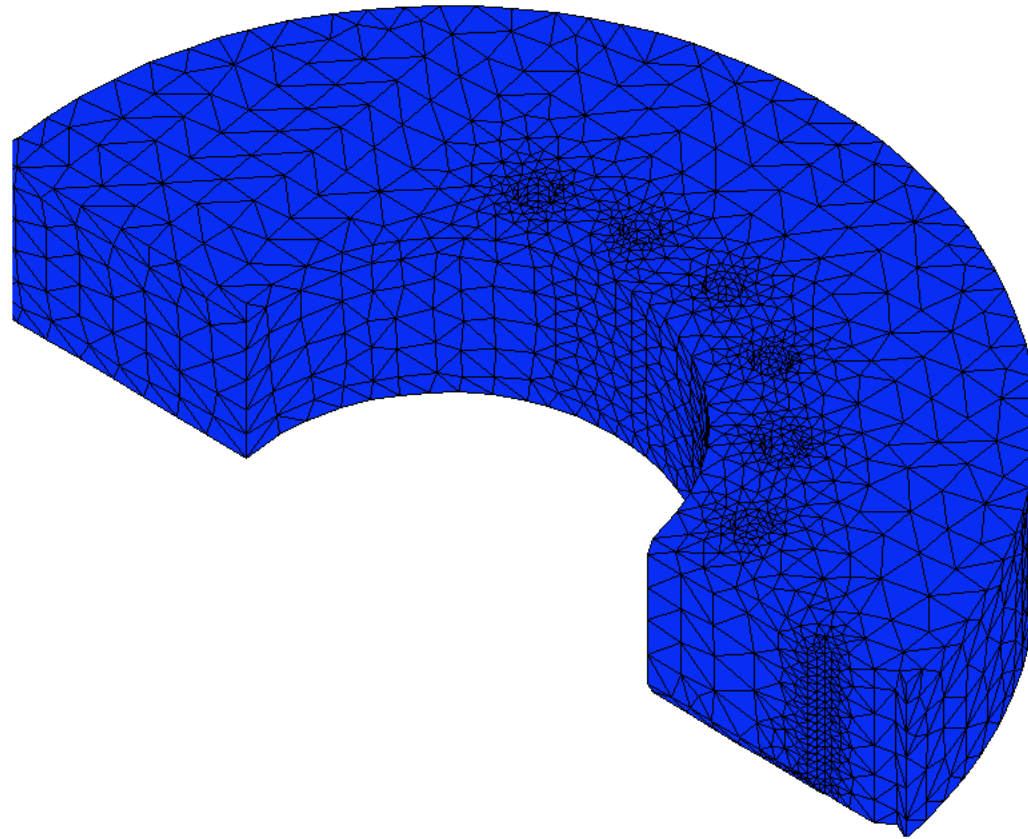
Maximiser la projection de $\underline{\varphi}(x)$
sur l'ensemble des
réponses $\underline{U}(x, t)$



Snapshot POD (Sirovich1987):
prendre un échantillon de l'état à quelques instants

Exemple : transitoire thermique à l'instant t_o $\beta = 1 \dots 40$

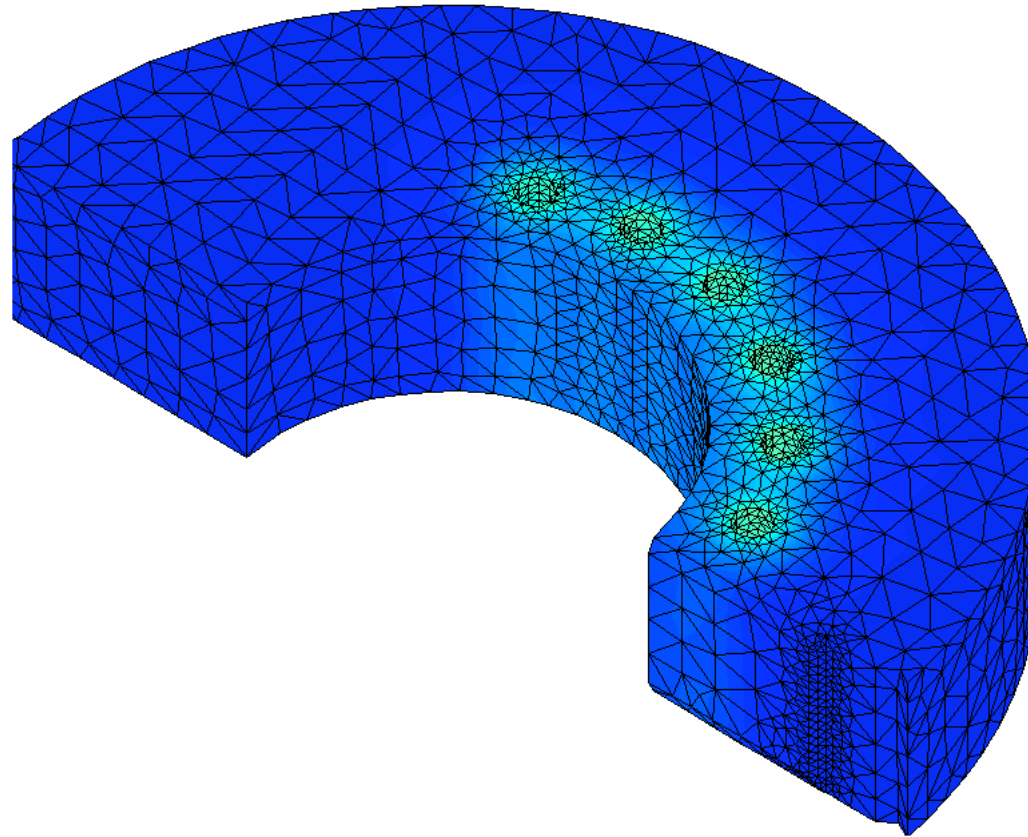
$\beta = 1$



Problème non linéaire : $C_p(T)$, $k(T)$, $h(T)$

Exemple : transitoire thermique à l'instant t_β $\beta = 1 \dots 40$

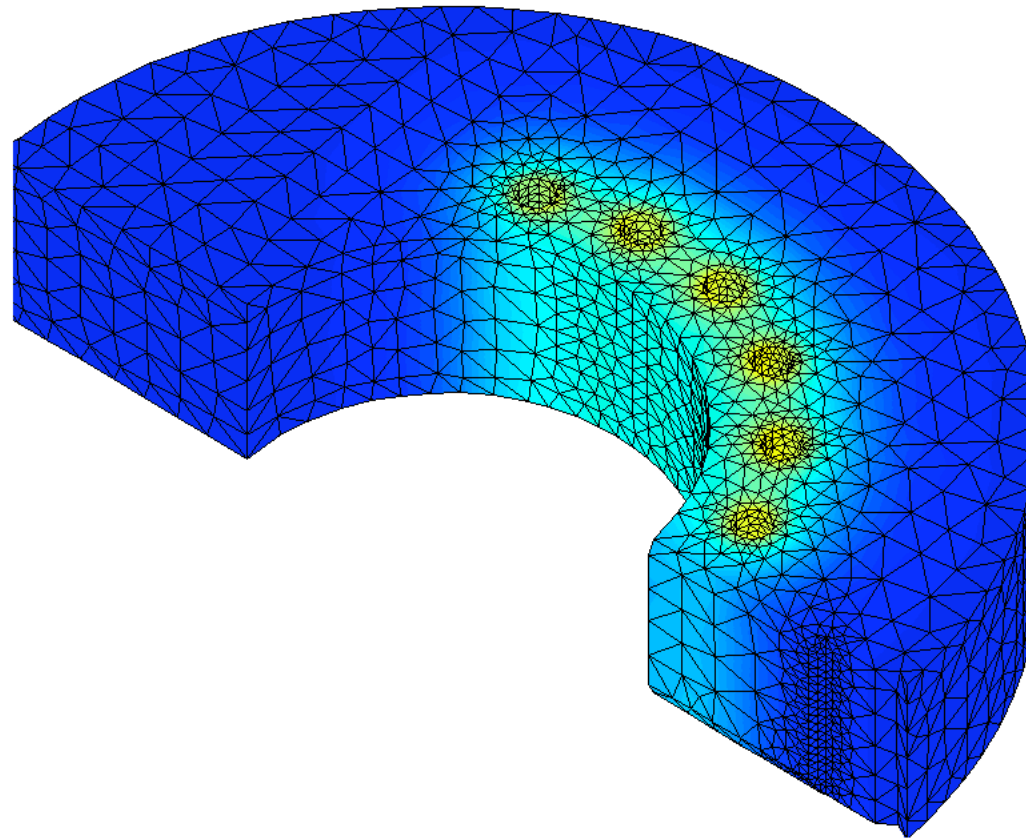
$\beta = 10$



Problème non linéaire : $C_p(T)$, $k(T)$, $h(T)$

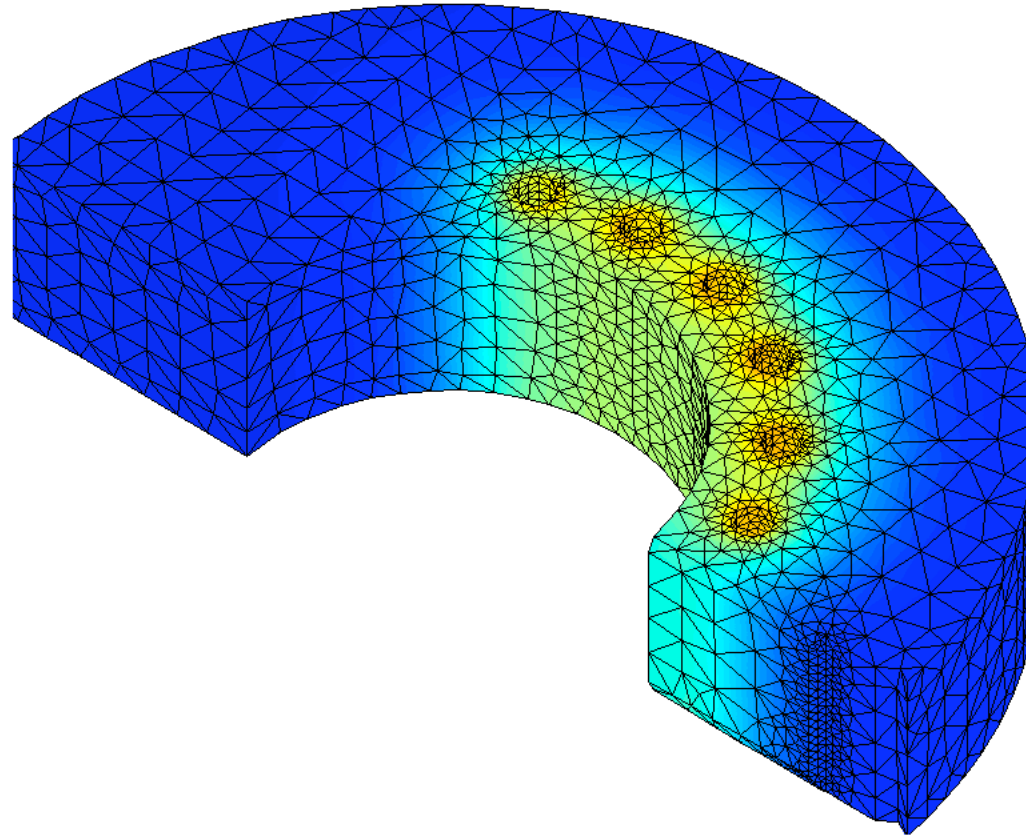
Exemple : transitoire thermique à l'instant t_β $\beta = 1 \dots 40$

$\beta = 20$



Problème non linéaire : $C_p(T)$, $k(T)$, $h(T)$

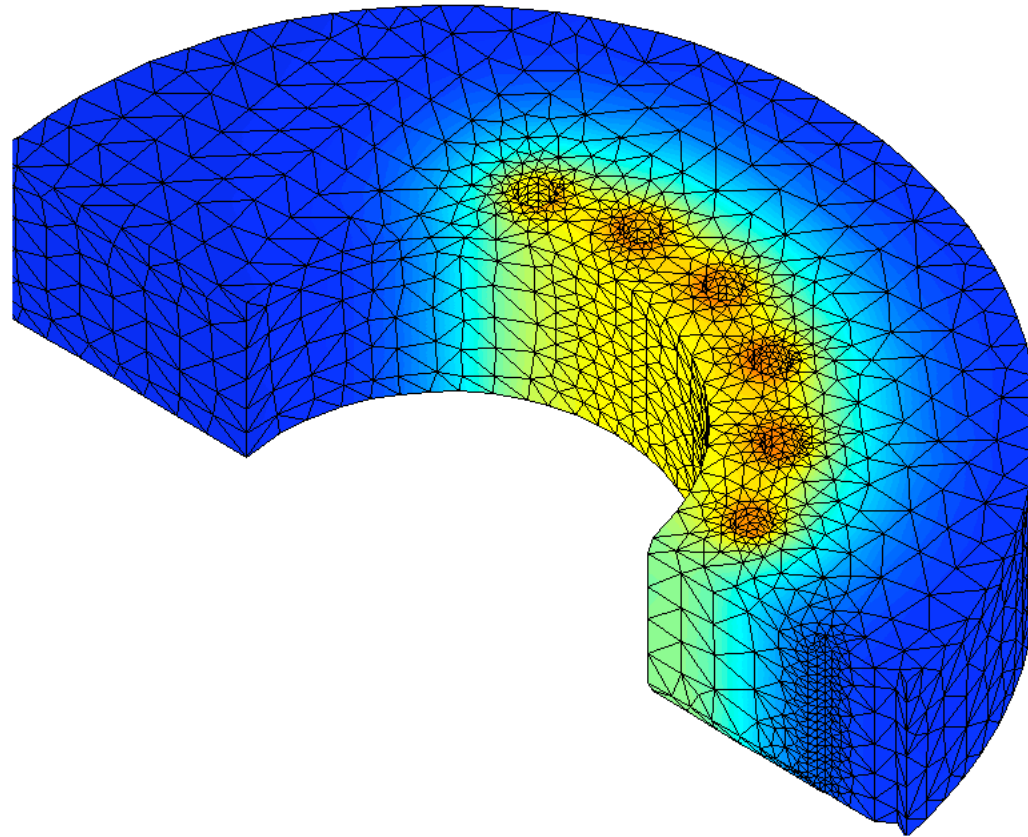
Exemple : transitoire thermique à l'instant t_α $\beta = 1 \dots 40$
 $\beta = 30$



Problème non linéaire : $C_p(T)$, $k(T)$, $h(T)$

Exemple : transitoire thermique à l'instant t_β $\beta = 1 \dots 40$

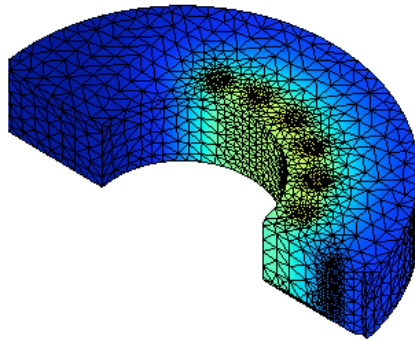
$\beta = 40$



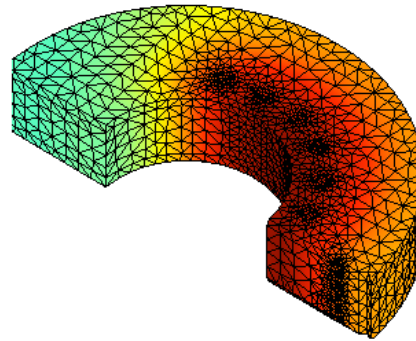
Problème non linéaire : $C_p(T)$, $k(T)$, $h(T)$

Exemple de fonctions de forme obtenues par la snapshot POD

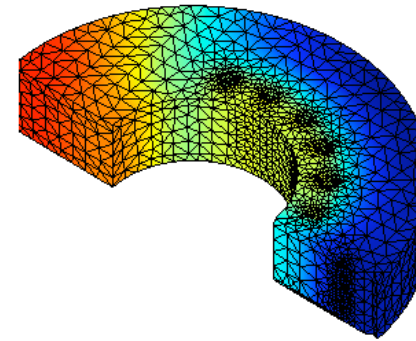
A_1



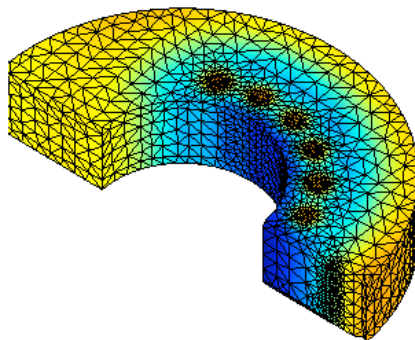
A_2



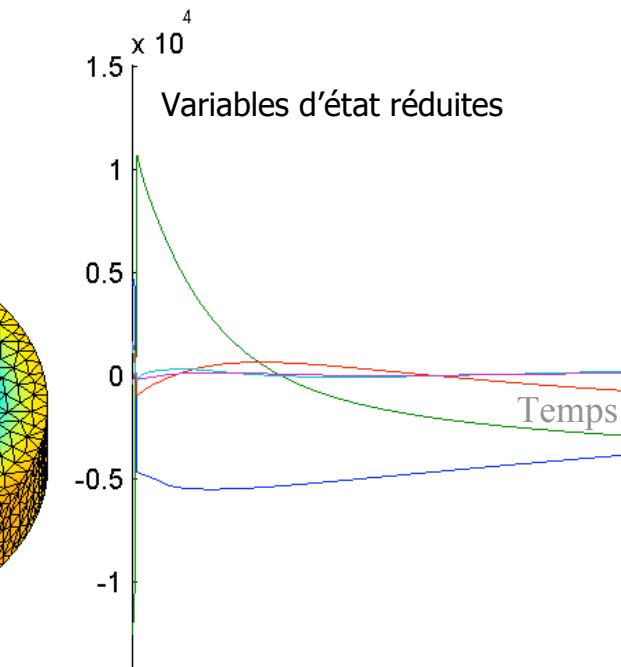
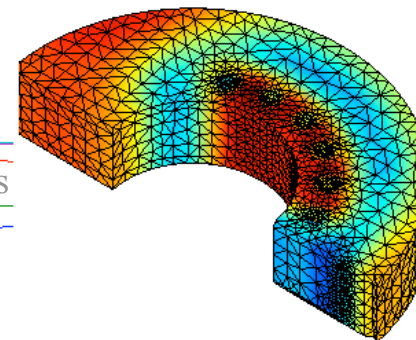
A_3



A_4



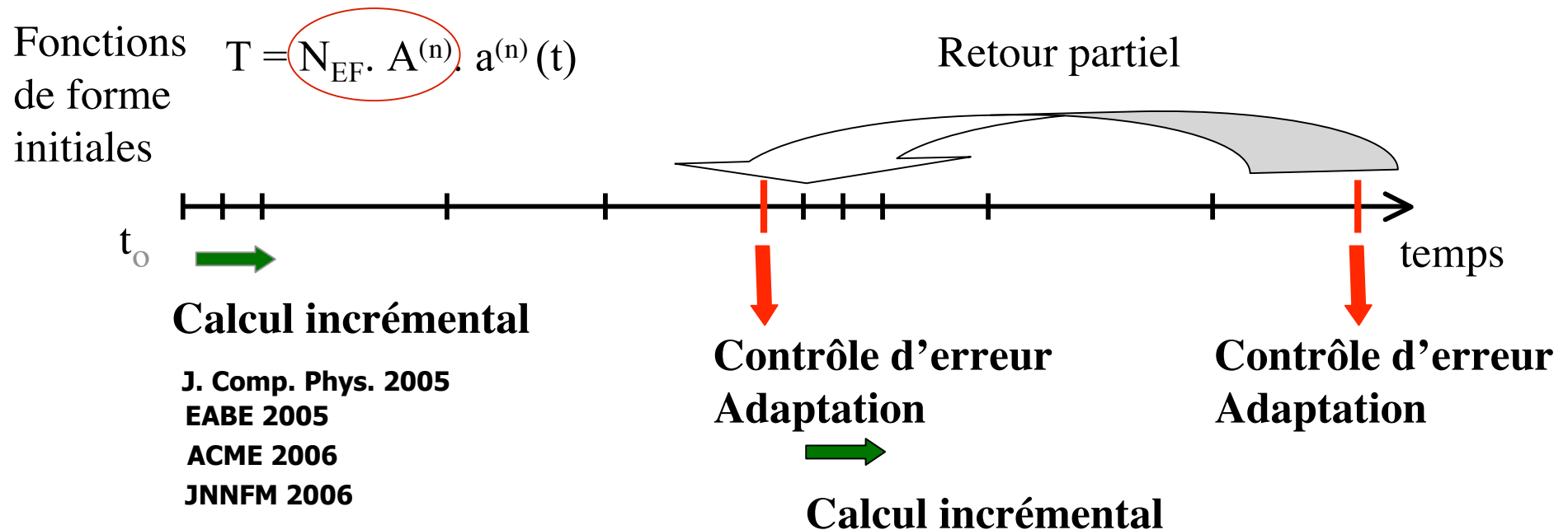
A_5



Régularité de l'évolution $\longrightarrow$ réduction

Comment adapter un modèle d'ordre réduit pour les problèmes d'évolution ?

Stratégie incrémentale d'adaptation des fonctions de forme pour la maîtrise des erreurs de discrétisation



Méthode APHR A Priori Hyper Reduction

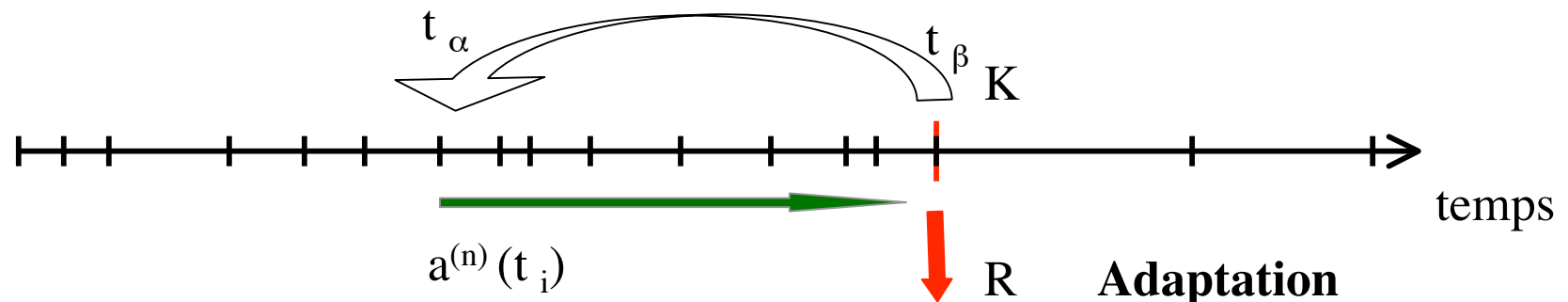
APHR = Snapshot POD + adaptation + ...

Calcul en base réduite entre deux “snapshots”

Retour partiel $\|R\| > \varepsilon \|F\|$

A Priori

$$A^{(0)} = \emptyset$$



$$V^{(n)} = \text{POD} (a^{(n)})$$

$$A^{(n+1)} = [A^{(n)} V^{(n)} , B]$$

Résol. E.F.

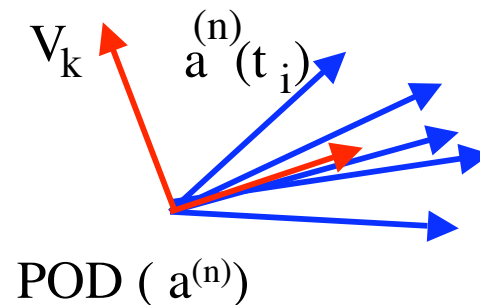
$$B = \delta q$$

Sous-espace de Krylov

$$B = [R , K R , K^2 R]$$

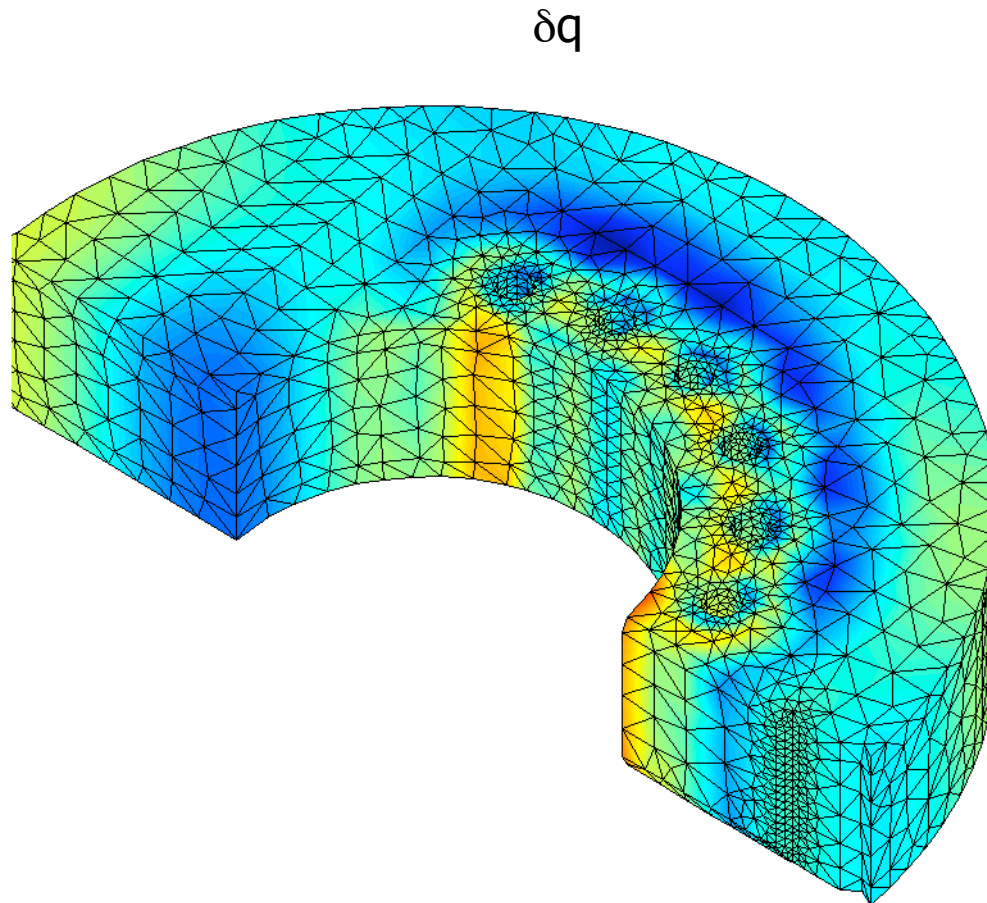
**EABE 2005
ACME 2006**

**J. Comp. Phys. 2005
JNNFM 2006**



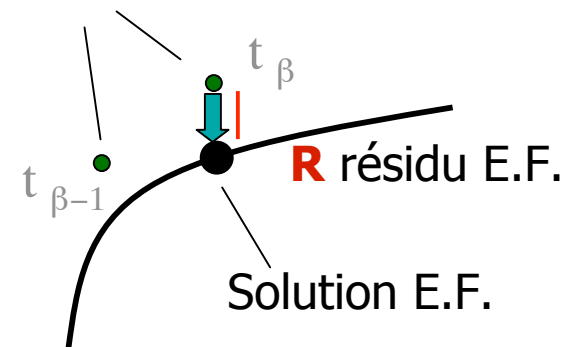
Actualisation $a^{(n+1)}$

Exemple de fonction de forme rajoutée pour l'extension de la base réduite



Fonction issue d'un calcul E.F. non-linéaire
sur un incrément en temps

Prévisions APHR (acc. Cv)



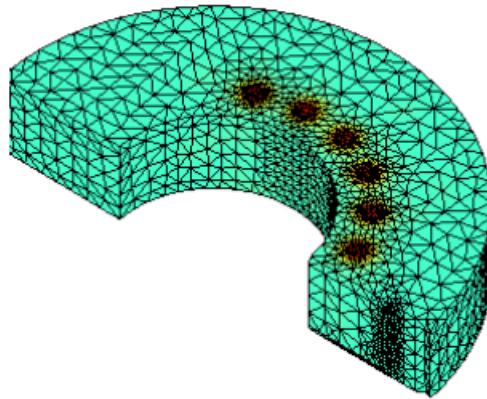
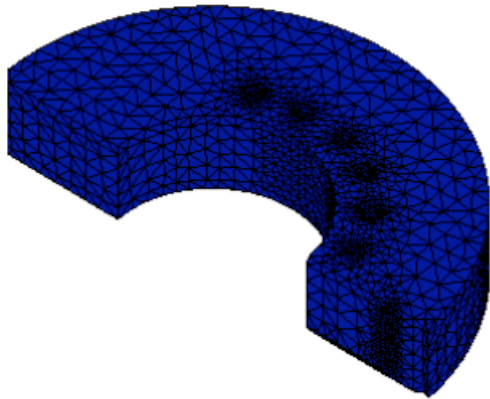
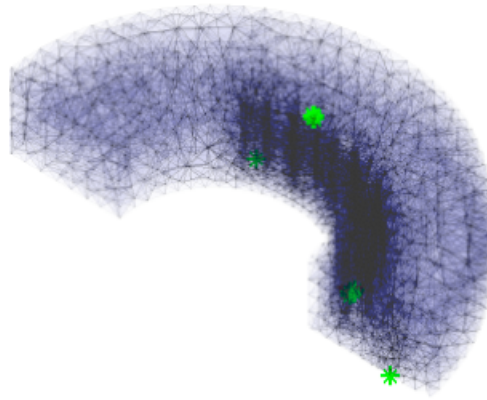
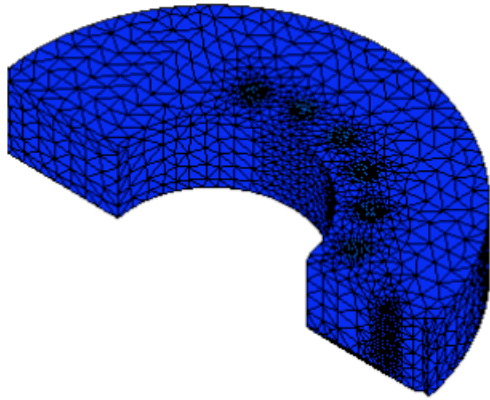
$$\delta q = q_{EF} - A^{(n)} (A^{(n)T} A^{(n)})^{-1} A^{(n)T} q_{EF}$$

Propriété :

$$A^{(n)T} \delta q = 0$$

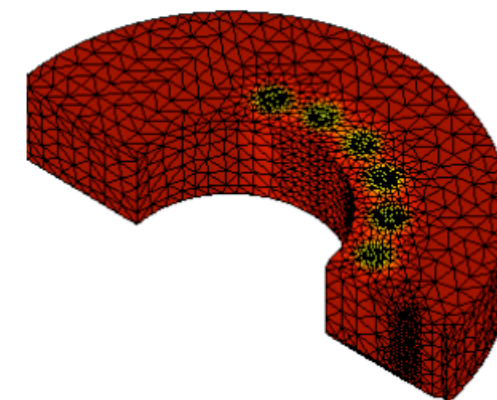
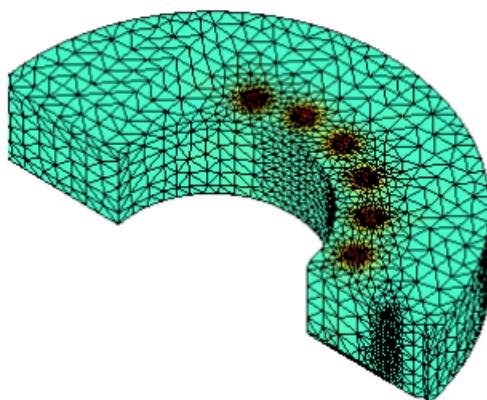
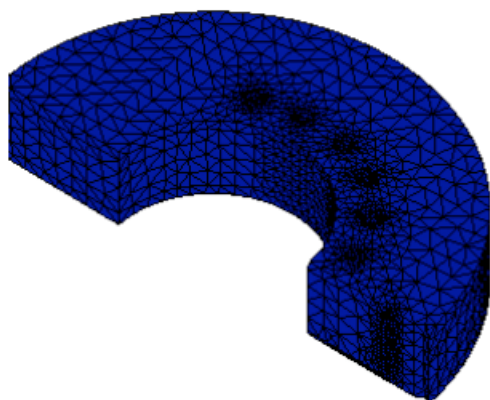
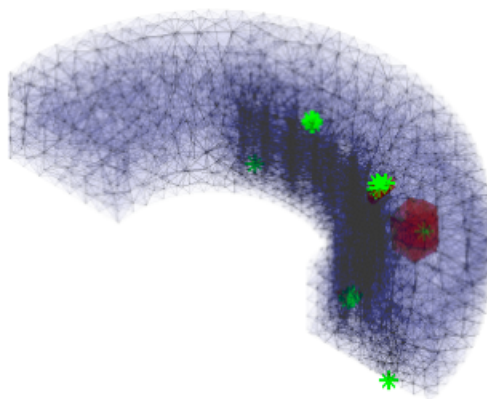
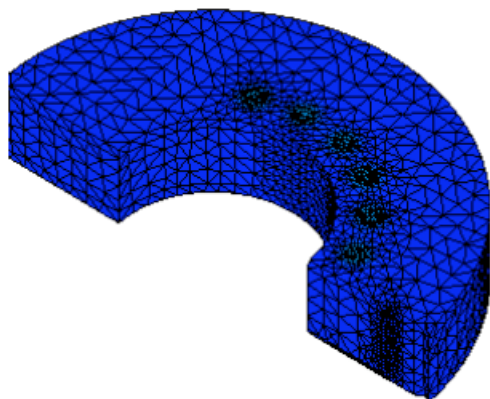
$\beta = 2$

2 fonctions de forme



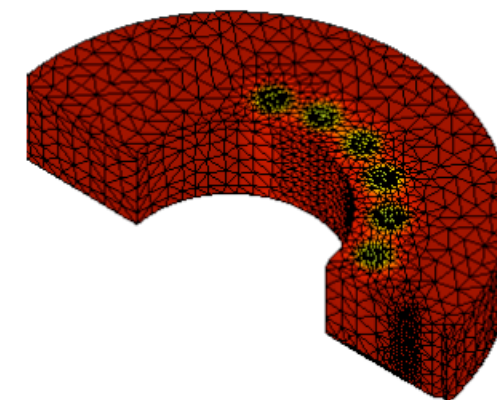
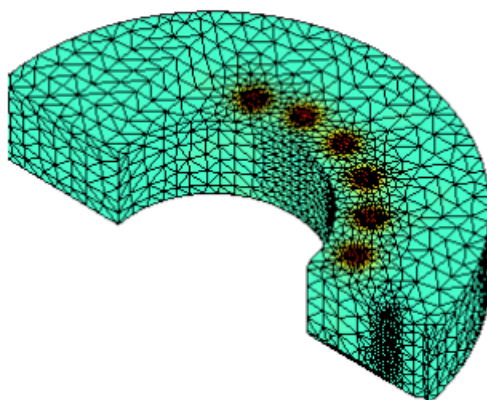
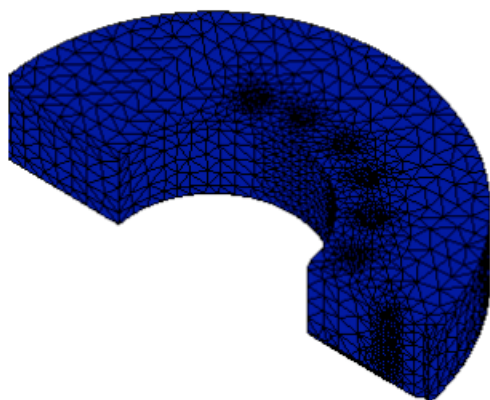
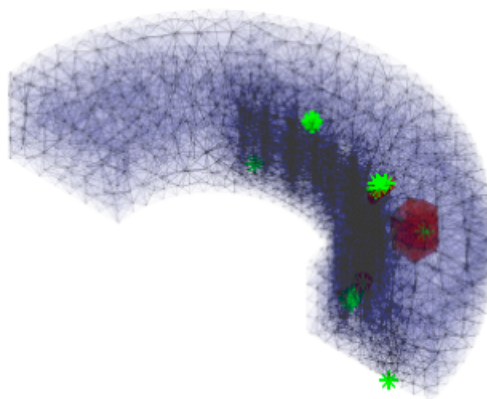
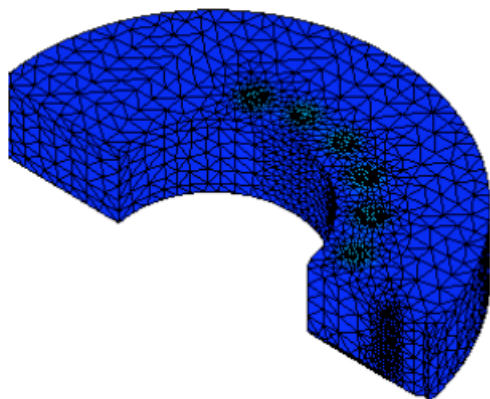
$\beta = 3$

3 fonctions de forme



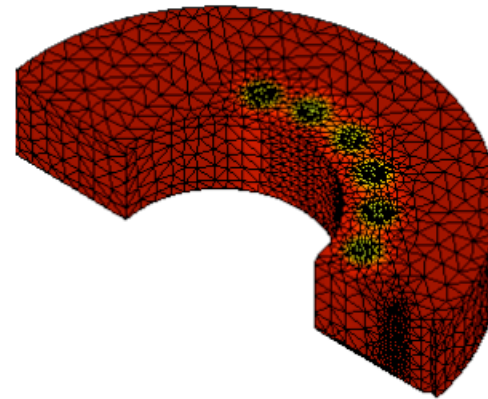
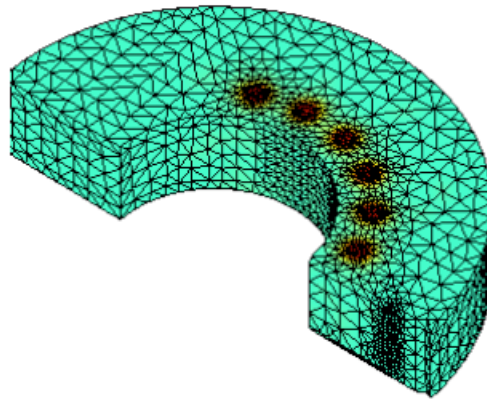
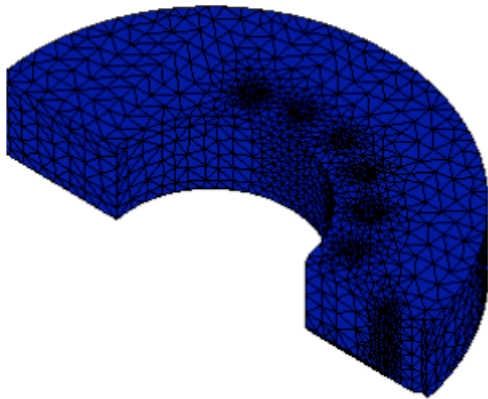
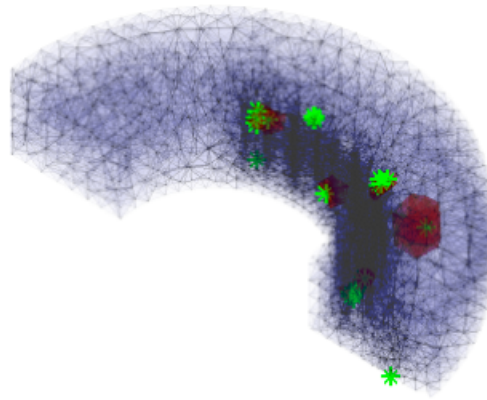
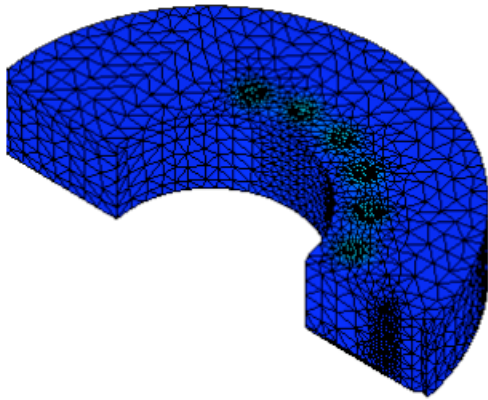
$\beta = 4$

4 fonctions de forme



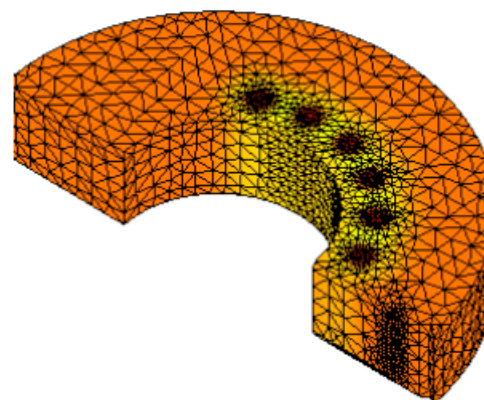
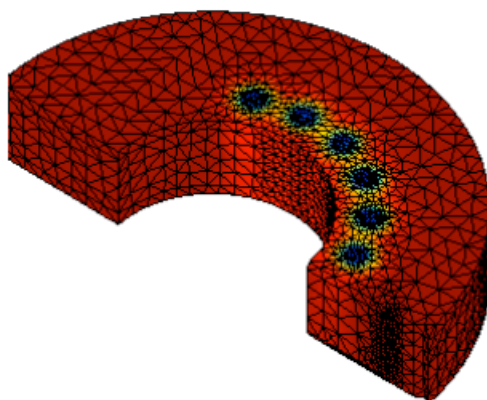
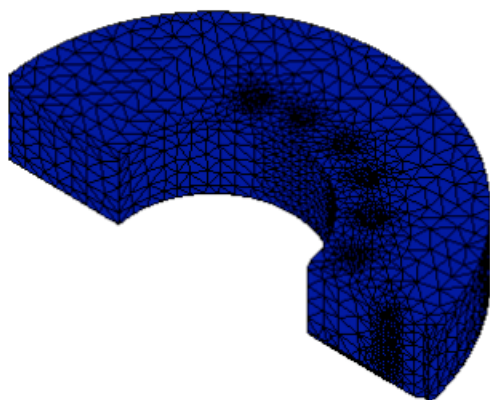
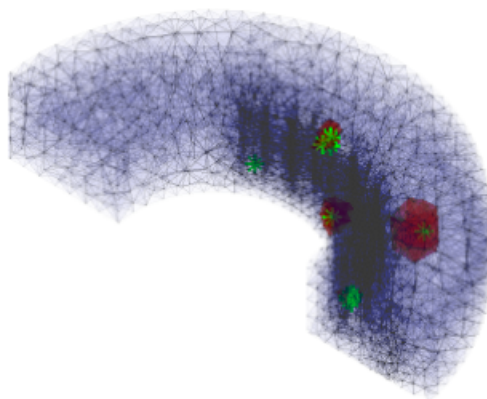
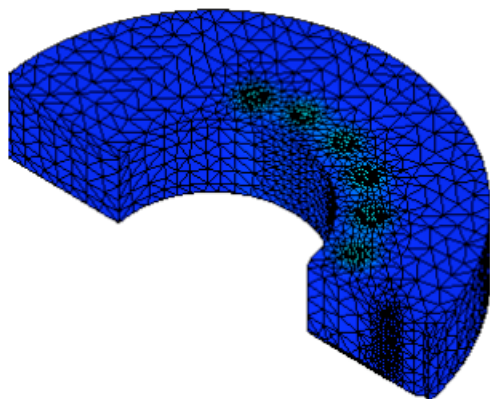
$\beta = 5$

5 fonctions de forme



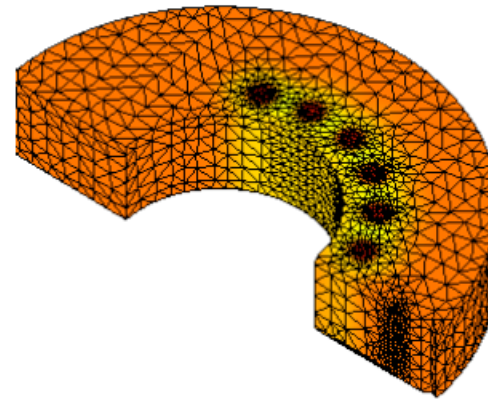
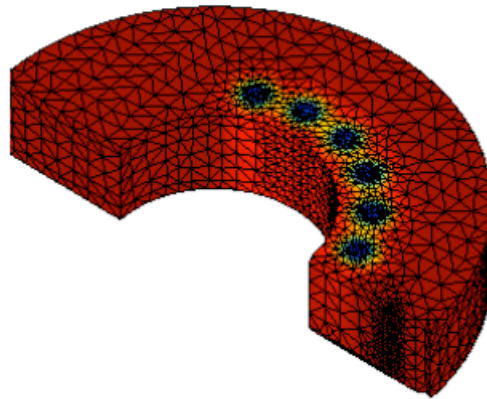
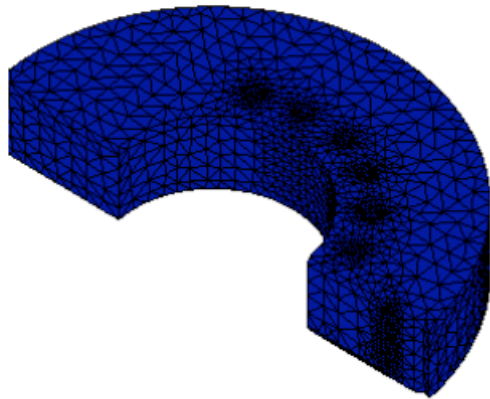
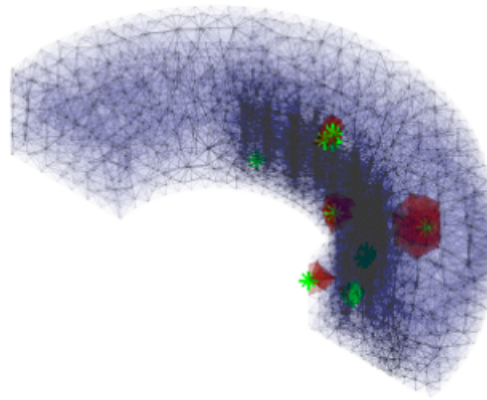
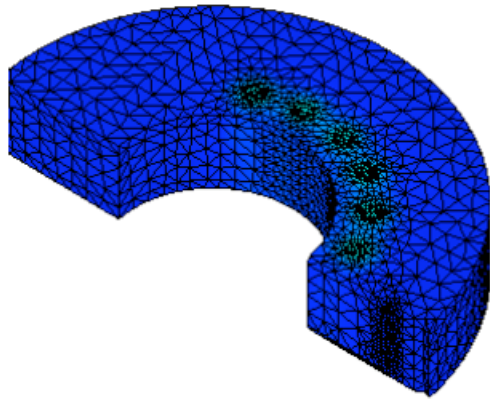
$\beta = 6$

4 fonctions de forme



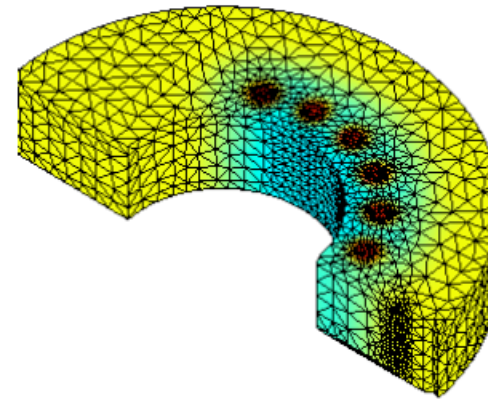
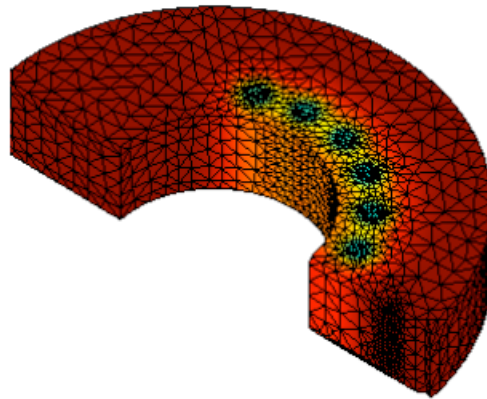
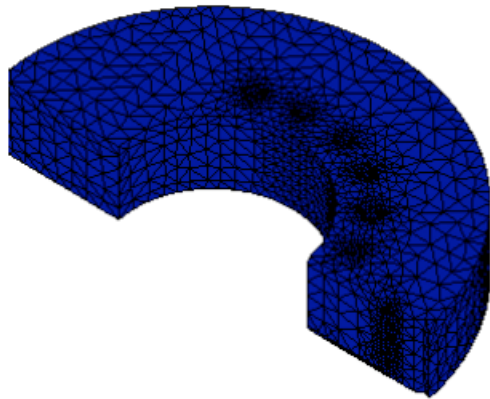
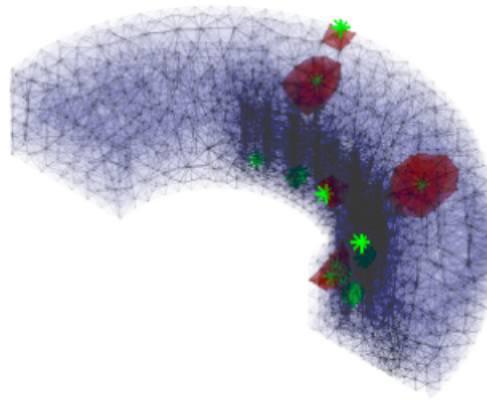
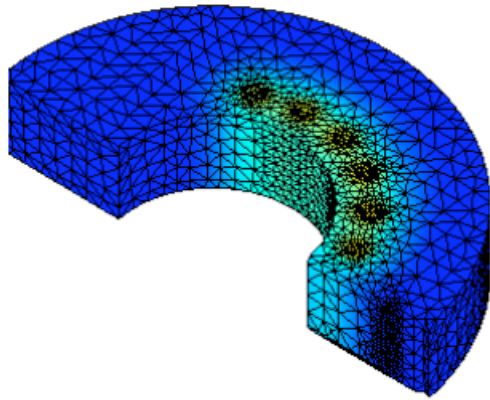
$\beta = 7$

5 fonctions de forme



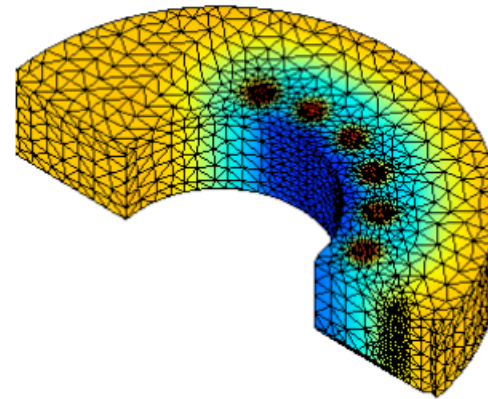
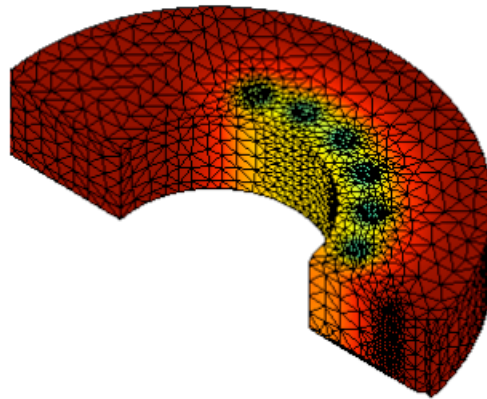
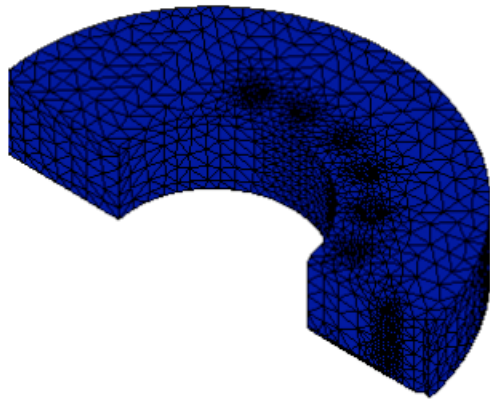
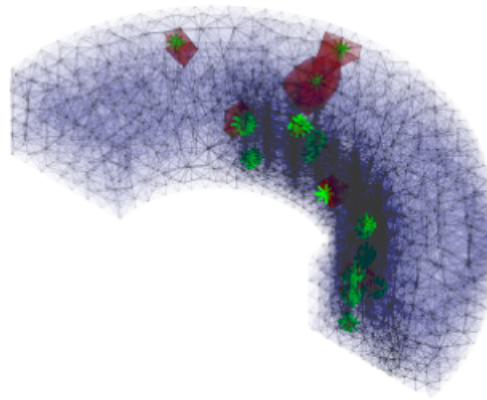
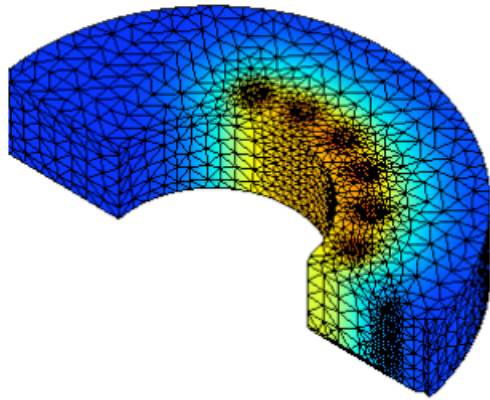
$\beta = 22$

6 fonctions de forme



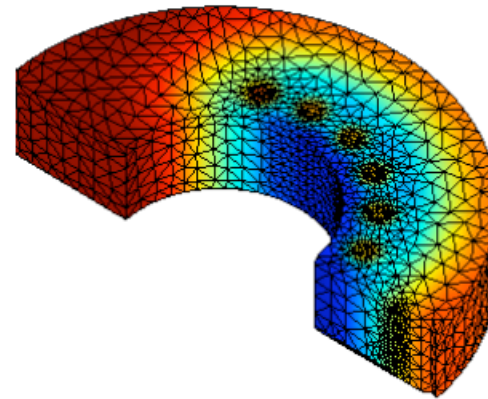
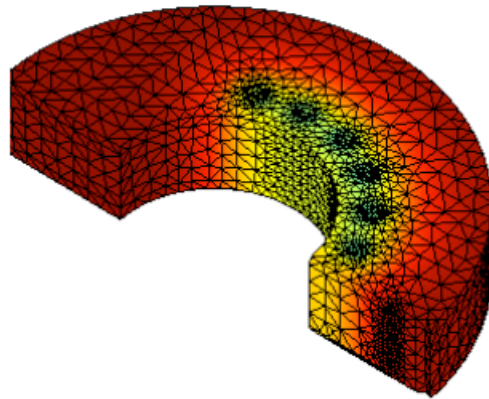
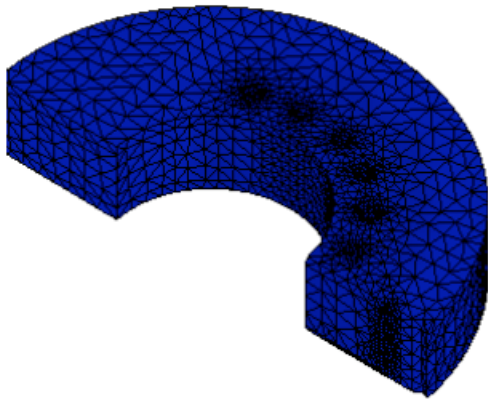
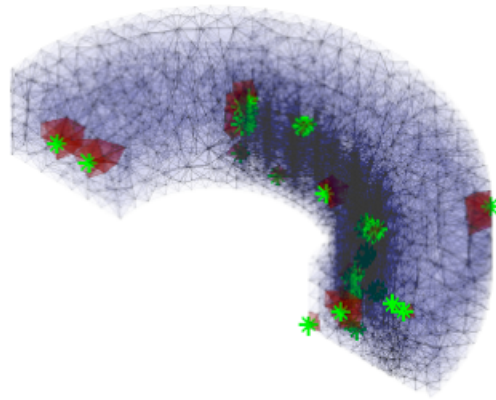
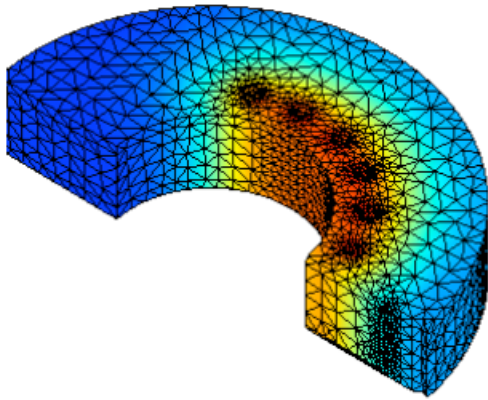
$\beta = 53$

11 fonctions de forme



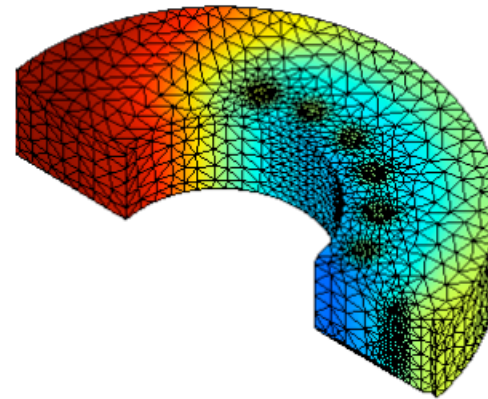
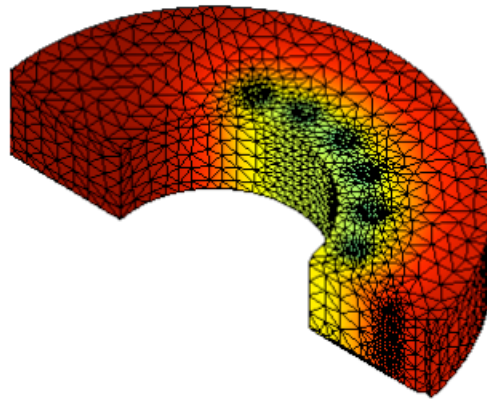
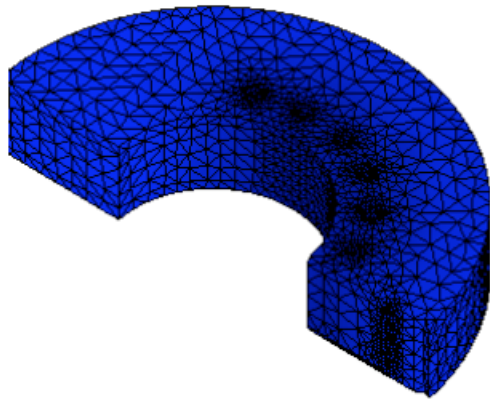
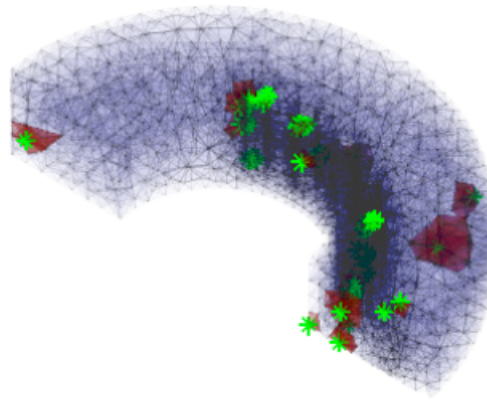
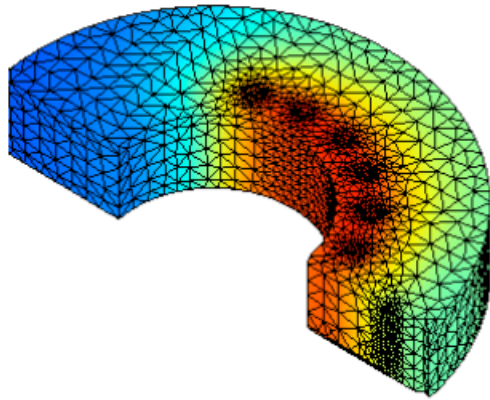
$\beta = 93$

13 fonctions de forme



$\beta = 184$

15 fonctions de forme

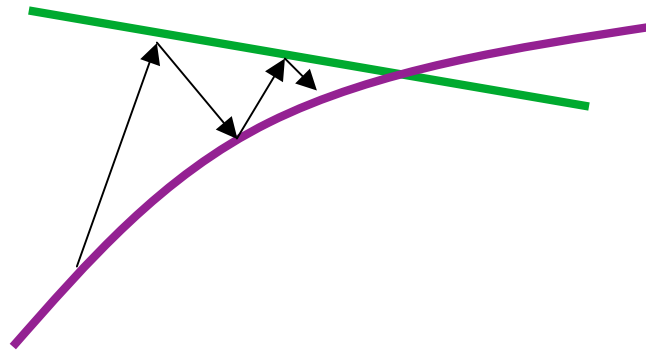


Problèmes non-linéaires :

équations **globales linéaires** + équations **non-linéaires locales**

Variables primales (U, T)

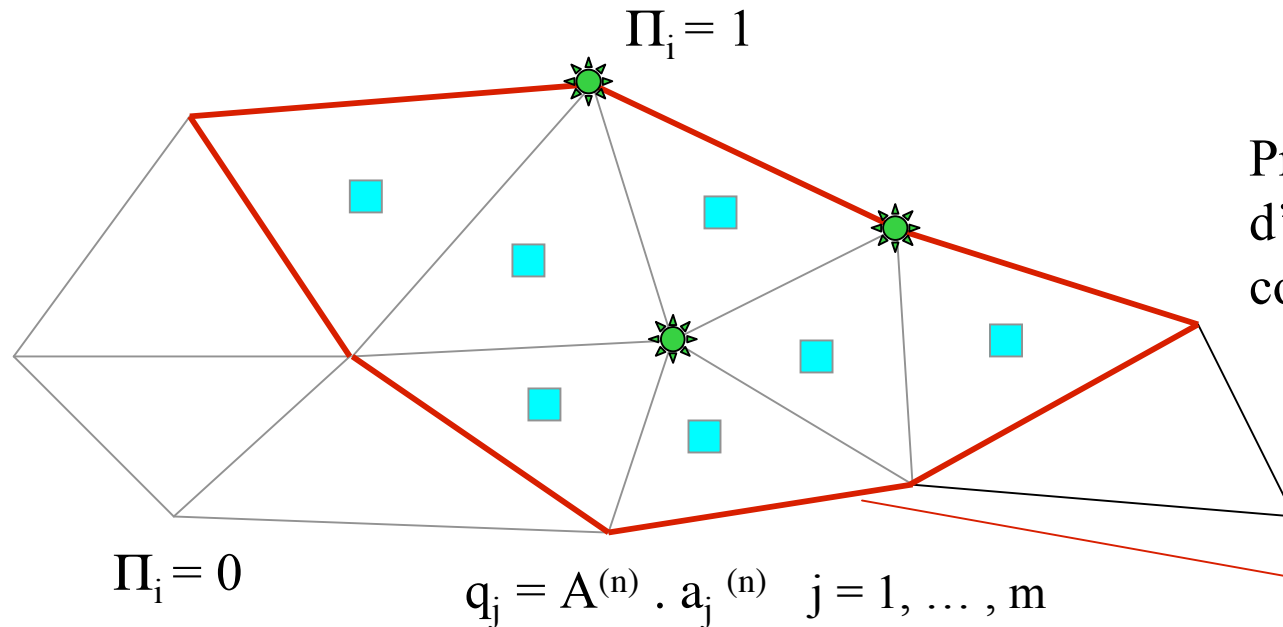
Variables internes ($p, \varepsilon^p, \dots$)



Les calculs locaux peuvent
représenter plus de 50% du temps
CPU!

Obtenir autant d'équations que de variables d'état réduites, sans Galerkin

★ ddl de contrôle des conditions d'équilibre du modèle complet $q^* = A^{(n)} \cdot a^*$



Propriété : Seuls les points d'intégration des éléments connectés sont nécessaires.

Sous-domaine isolé pour le calcul des variables d'état réduites

$$q^* = \Pi^T \cdot \Pi \cdot A^{(n)} \cdot a^* \quad \star$$

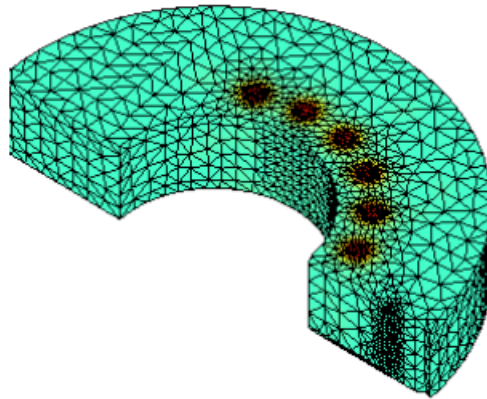
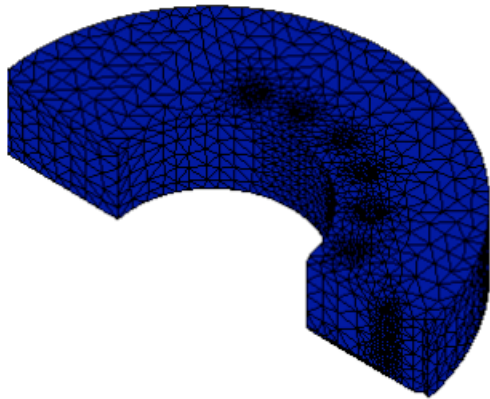
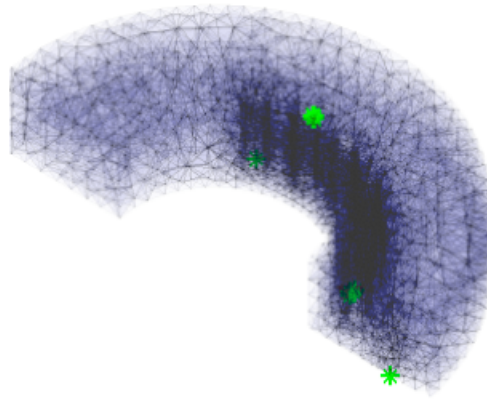
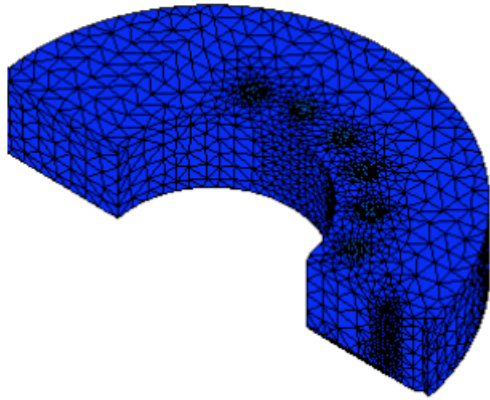
$$A^{(n)T} \cdot \Pi^T \cdot \Pi \cdot R(A^{(n)} \cdot a_{j+1}^{(n)}, A^{(n)} \cdot a_j^{(n)}) = 0 \quad j = 1, \dots, m-1$$

Formulation du type Petrov-Galerkin

APHR = Snapshot POD + adaptation + hyper réduction

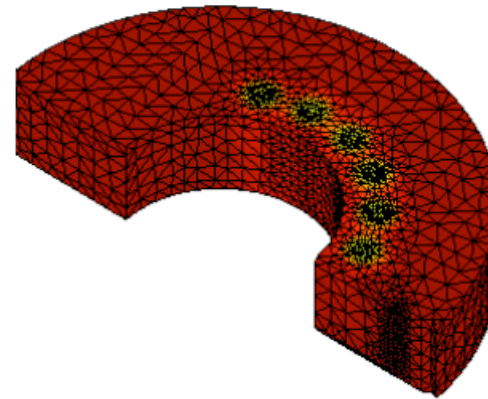
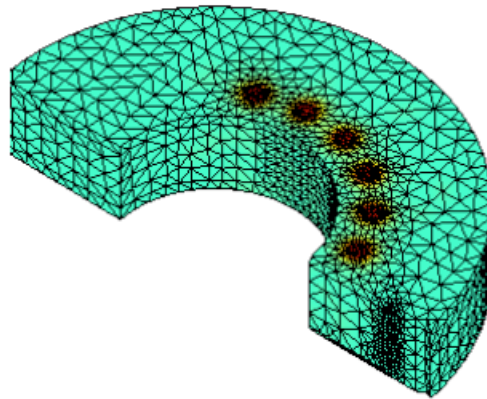
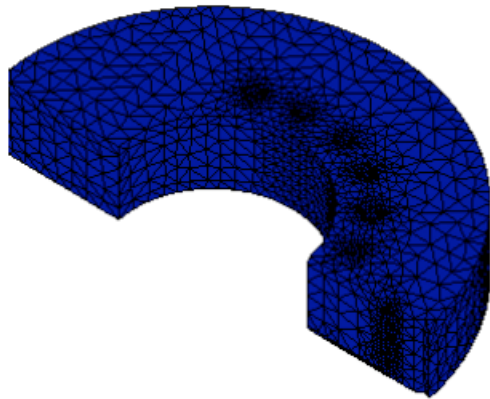
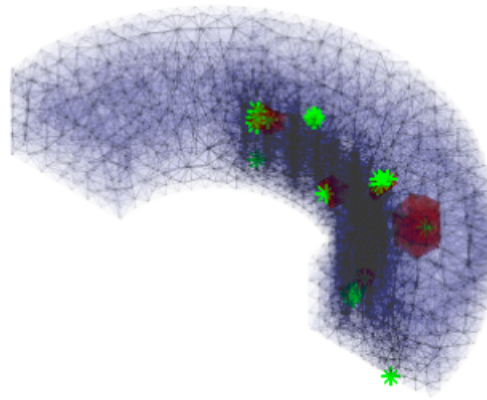
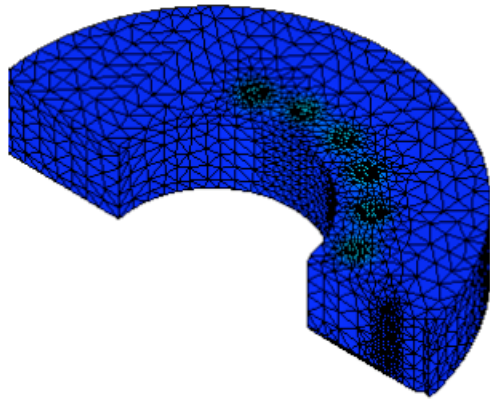
$\beta = 2$

2 fonctions de forme



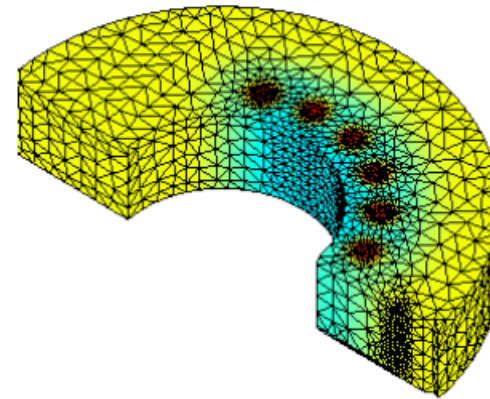
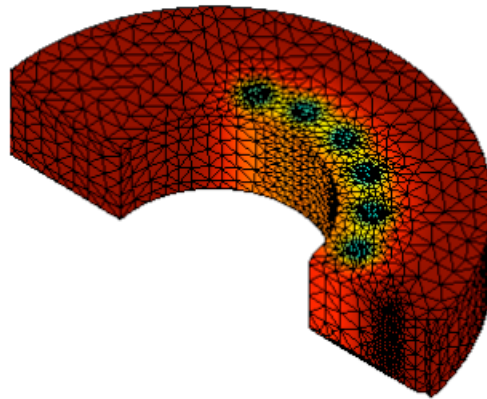
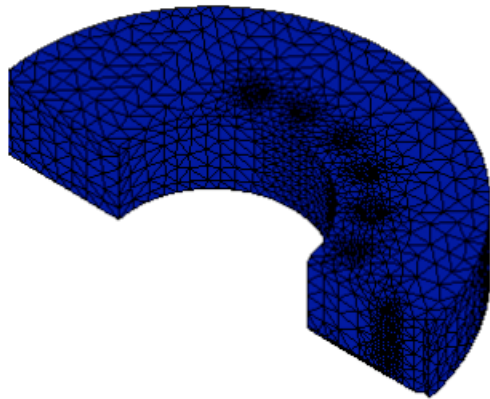
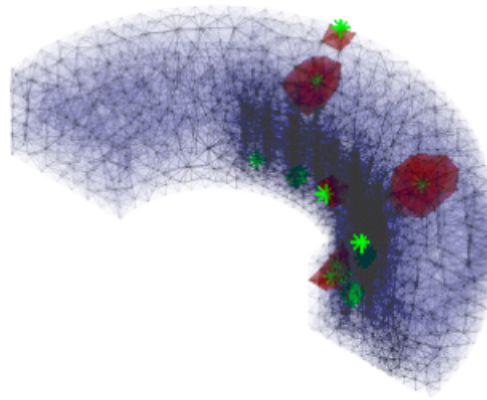
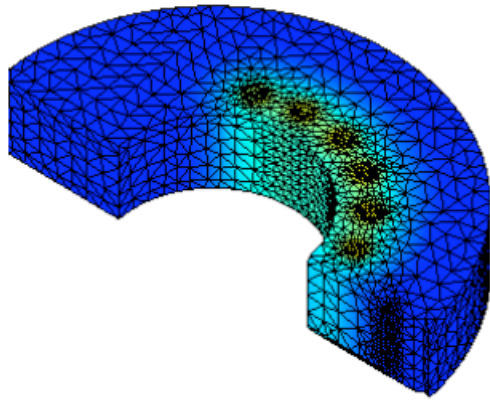
$\beta = 5$

5 fonctions de forme



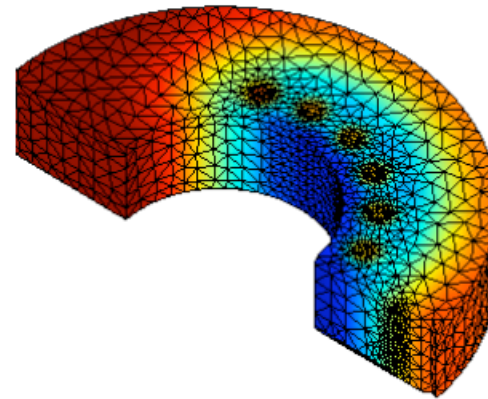
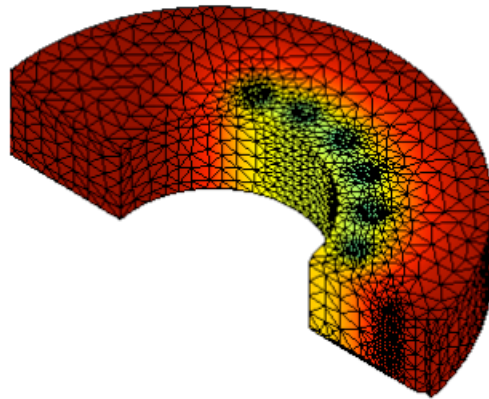
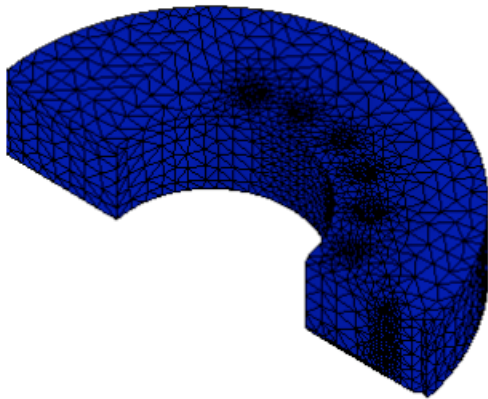
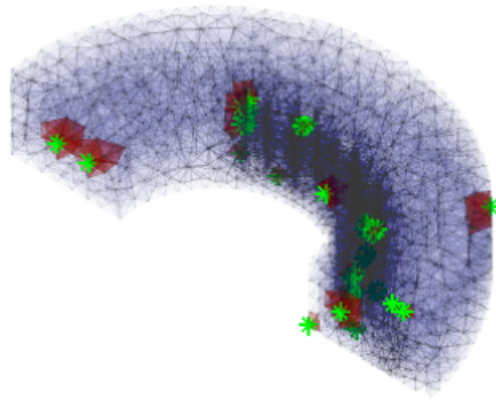
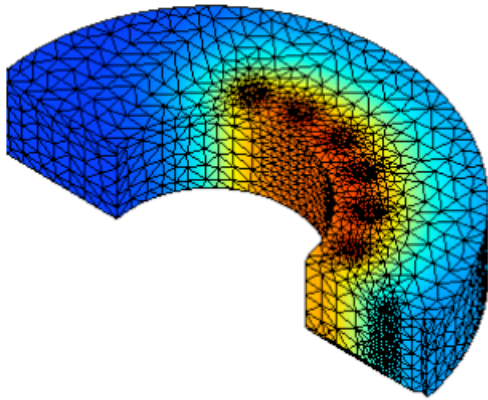
$\beta = 22$

6 fonctions de forme



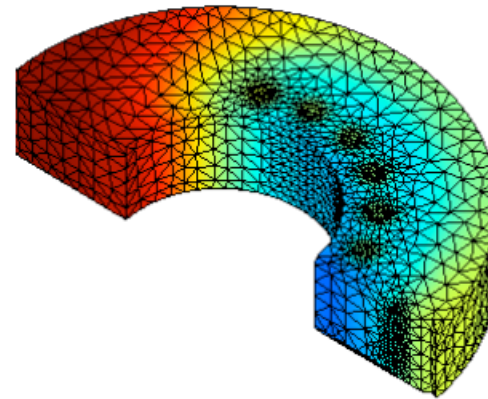
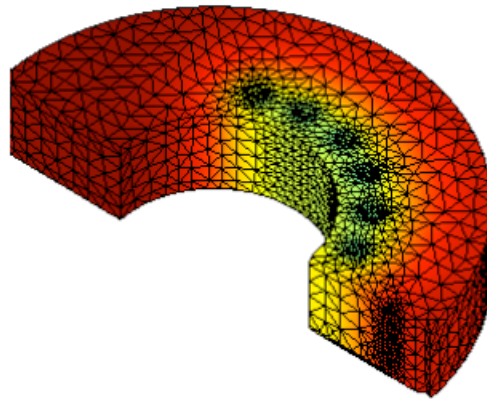
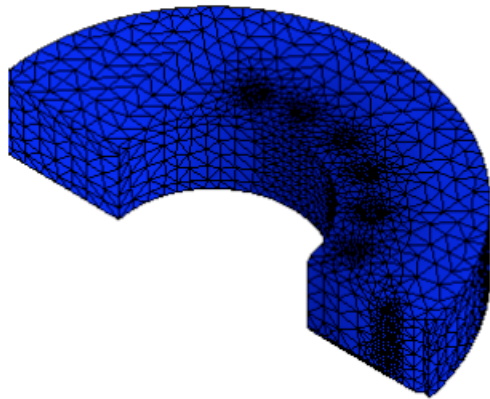
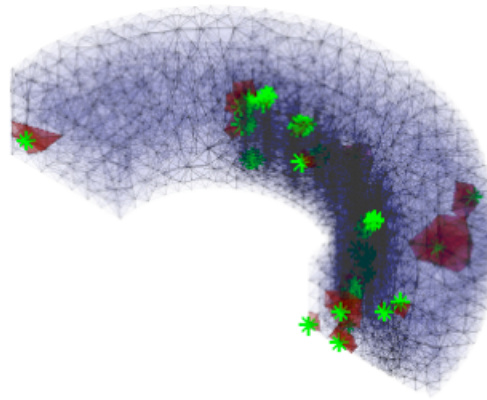
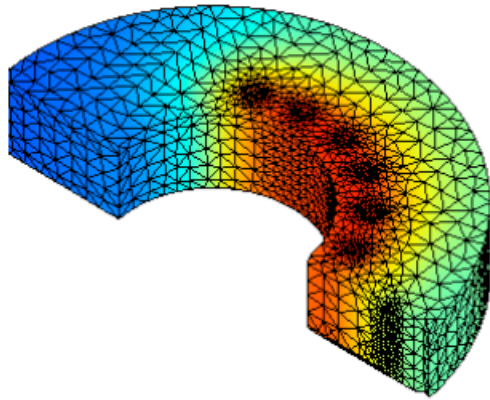
$\beta = 93$

13 fonctions de forme



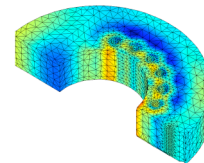
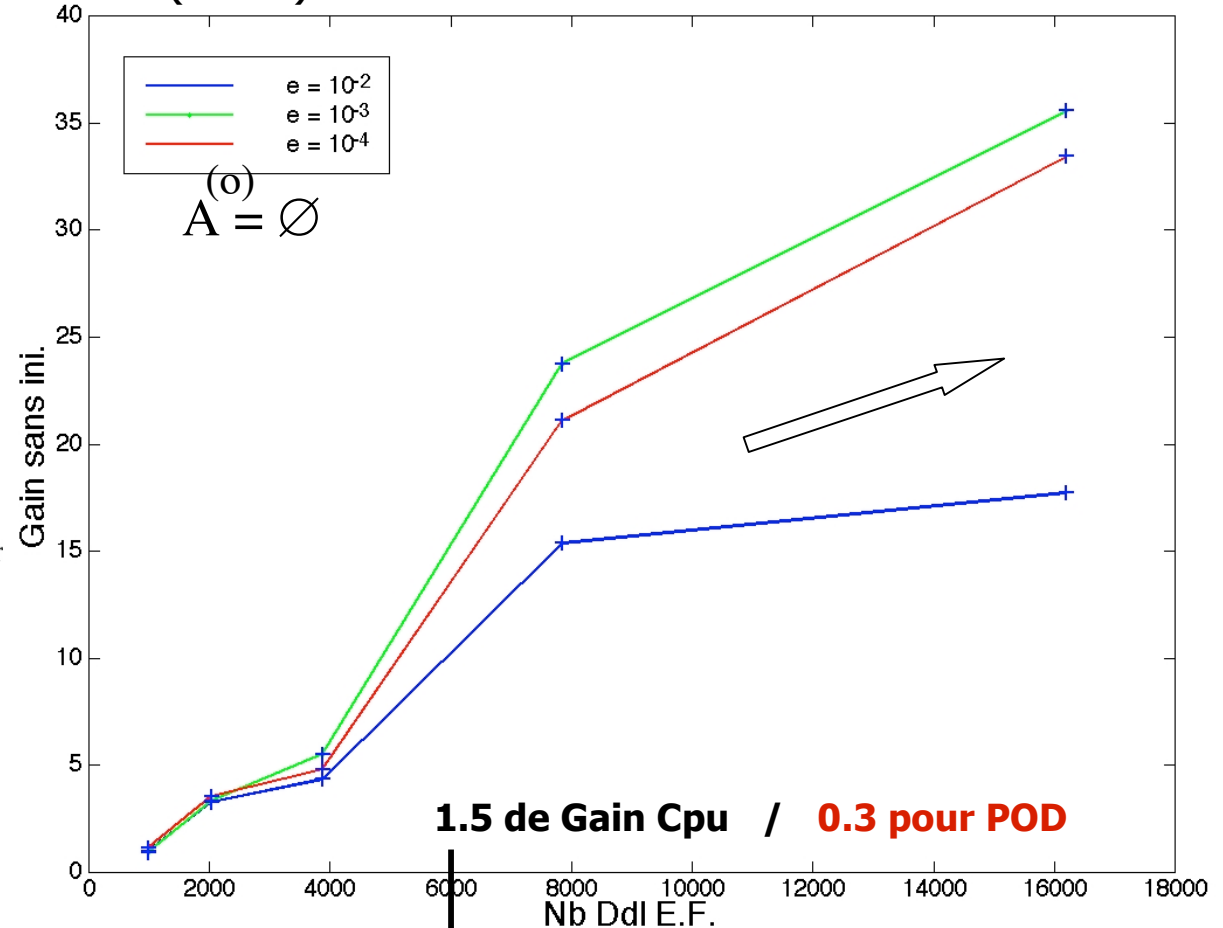
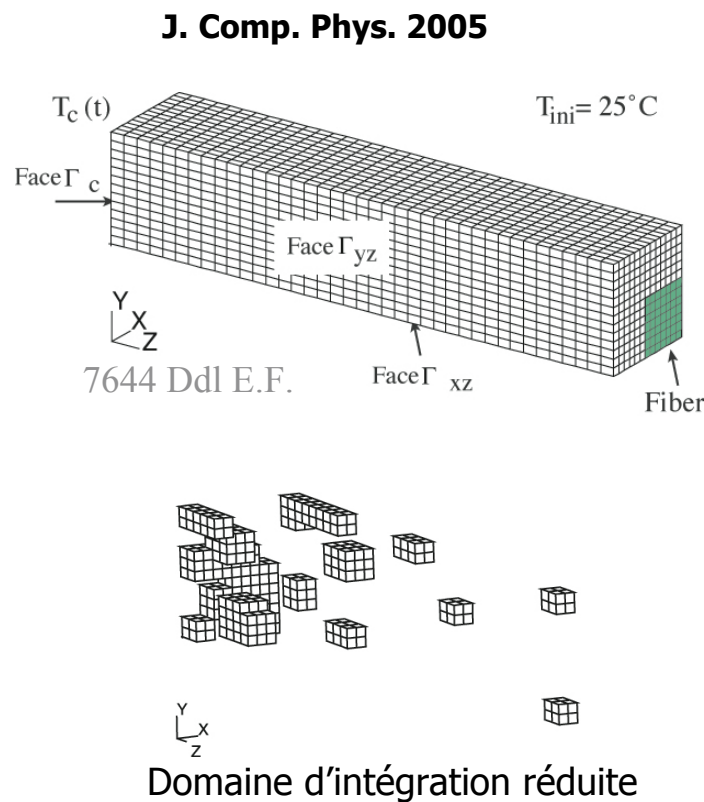
$\beta = 184$

15 fonctions de forme



Analyse de la complexité de la stratégie adaptative de réduction de modèles

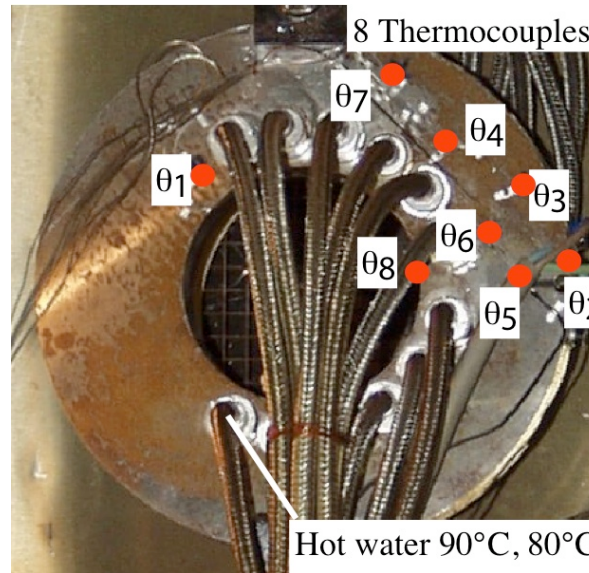
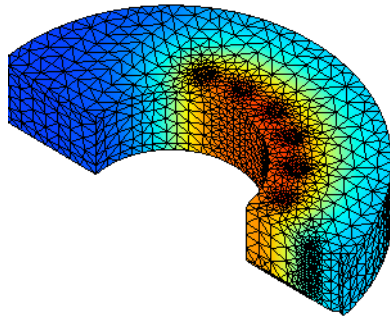
Gain/EF (FLOP)



6000 $\Rightarrow$ 15 variables d'état
25000 $\Rightarrow$ 800 éléments

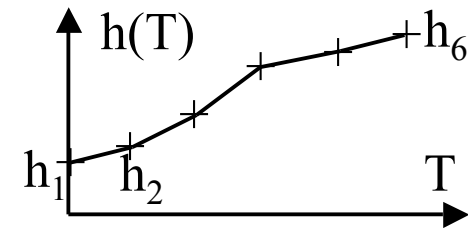
Exemple de problème inverse traité avec la méthode APHR

Thermal shock modeling

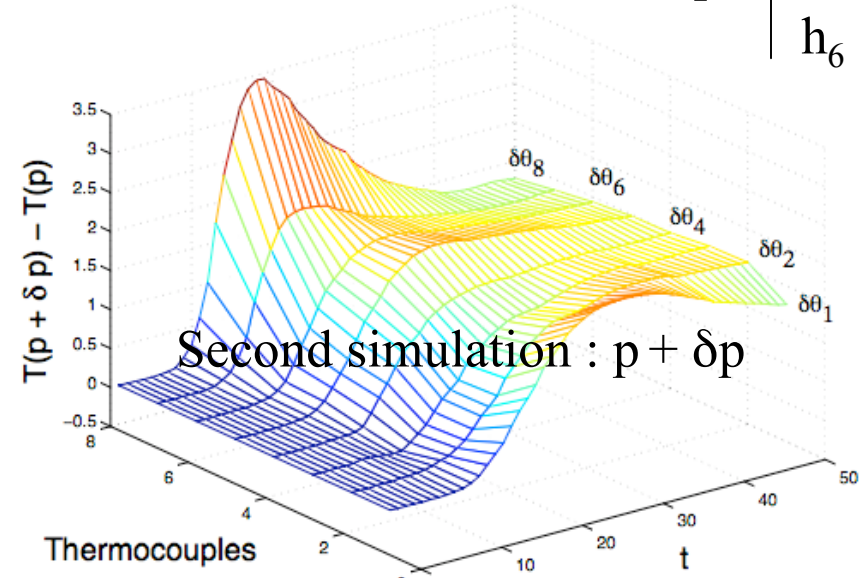
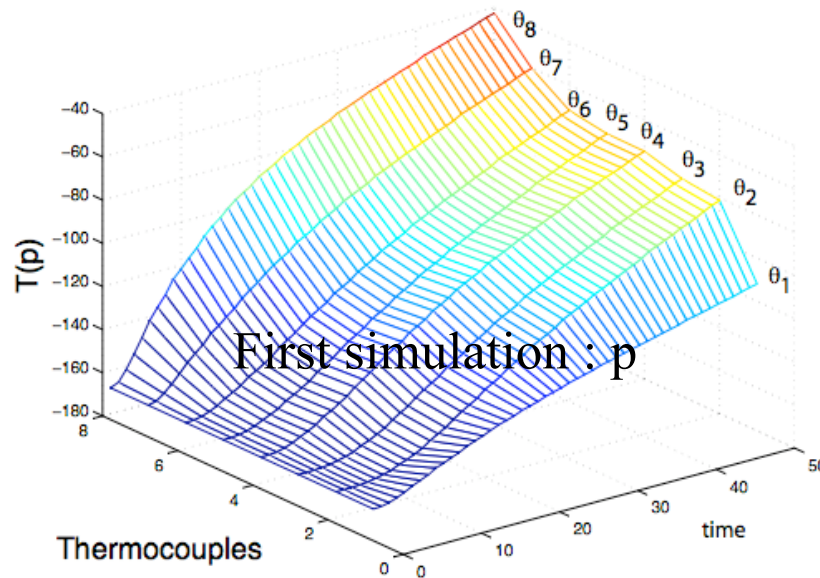


Goal function : $\| \theta(p) - \theta_{\text{exp}} \|$

Thermal transfer coefficient



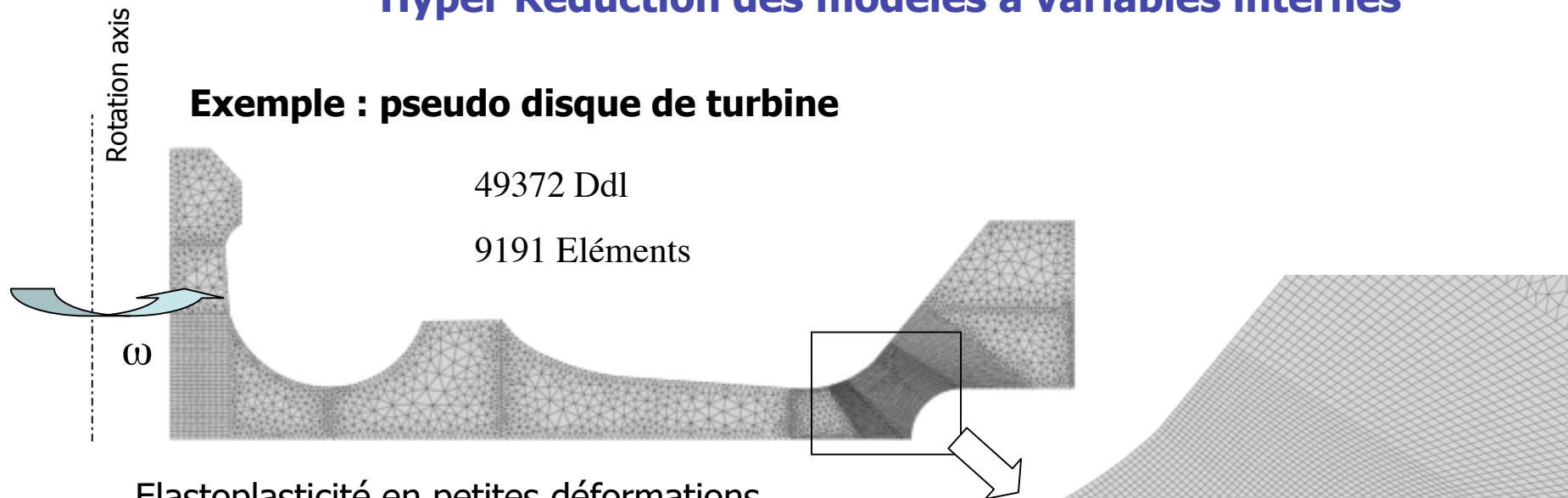
$$p = \begin{pmatrix} h_1 \\ h_2 \\ \dots \\ h_6 \end{pmatrix}$$



Different shapes of state evolutions : **Adaptivity is necessary**

Hyper Réduction des modèles à variables internes

Exemple : pseudo disque de turbine



Elastoplasticité en petites déformations
(modèle de Chaboche)

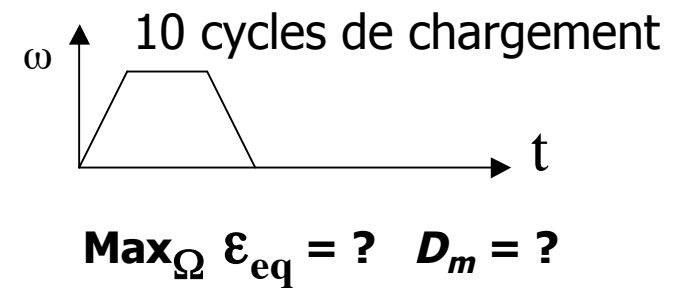
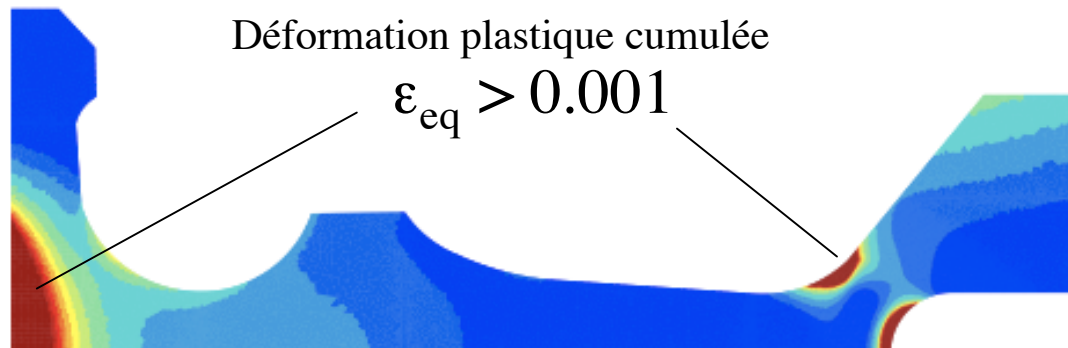
$$f(\sigma_{ij} - a_{ij}) = \sqrt{\frac{3}{2}(\tau_{ij} - \alpha_{ij})(\tau_{ij} - \alpha_{ij})} - \sigma_{y0} - R$$

$$R = Q(1 - e^{-bp})$$

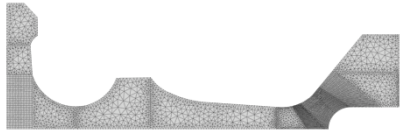
$$\dot{\epsilon}_{ij} = \dot{\epsilon}_{ij}^e + \dot{\epsilon}_{ij}^p \quad \dot{p} = |\dot{\epsilon}_{ij}^p| = \left[\frac{2}{3} \dot{\epsilon}_{ij}^p \dot{\epsilon}_{ij}^p \right]^{1/2}$$

$$\dot{\alpha}_{ij} = \sum_{k=1}^n (\dot{\alpha}_{ij})_k = \sum_{k=1}^n \left(\frac{2}{3} C_k \dot{\epsilon}_{ij}^p - \gamma_k (\alpha_{ij})_k \dot{p} \right) \quad n = 3$$

Matériau
TA6V



Facteur asymptotique de réduction du temps de calcul



Compute_internal_reac calls = 427 (160 x 3)
inc. x glob. iter.

Calls in Local Int = 14164871 (9191 x 160 x 3 x 3)
Elem. x inc. x glob. iter. x loc. iter.

Time CPU Total = 1555 s

Time Compute_internal_forces = 691 s

Time Modified Dscpack solver = **446** s

Si seul le nombre de ddl du modèle est réduit, alors le facteur asymptotique de réduction du temps de calcul est :

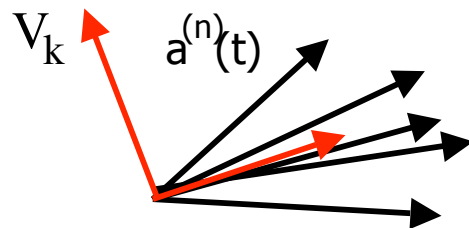
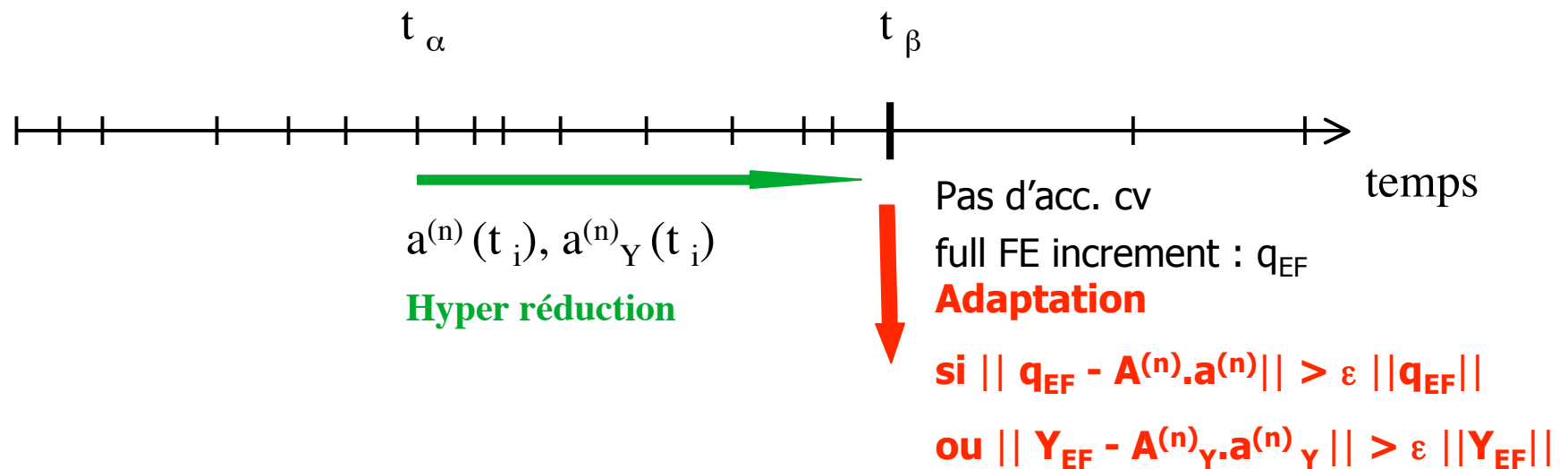
$$1.4 = \frac{1555}{1555 - 446} \quad \text{Pour un ROM connu}$$

Nous souhaitons améliorer ce facteur en réduisant le nombre de calculs locaux.

Construction de la base par un algorithme adaptatif

Calcul complet d'incrément uniquement pour adapter le modèle d'ordre réduit

A Priori
 $A^{(0)} = \emptyset$



Sélection par POD

$$V = \text{POD} (a^{(n)})$$

$$\delta q = q_{EF} - A^{(n)}.a^{(n)}$$

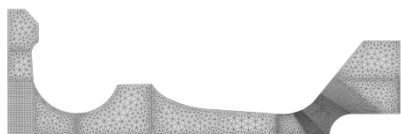
$$A^{(n+1)} = [A^{(n)} V , \delta q]$$

Sélection

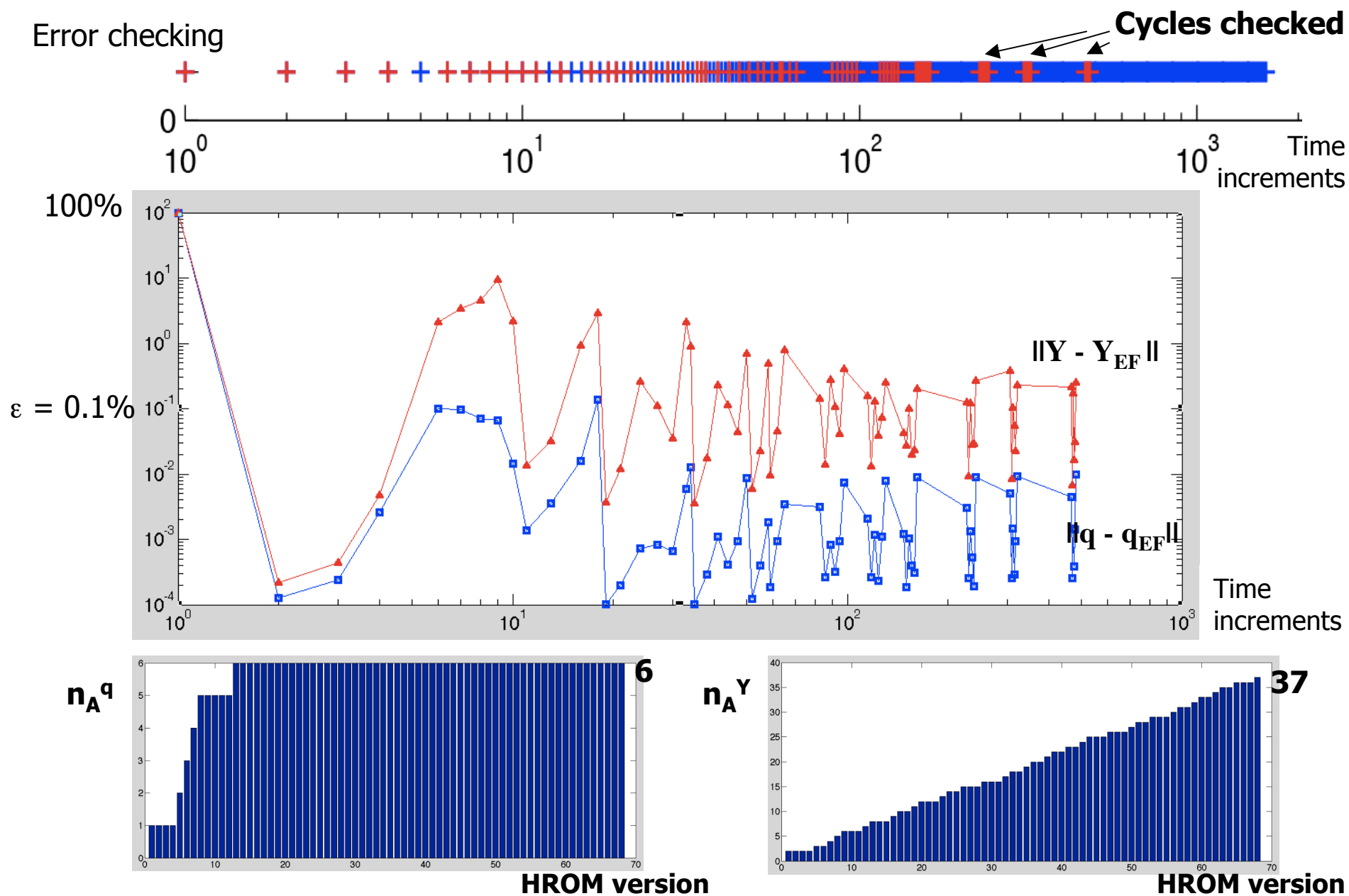
Extension

Actualisation

Détermination de t_β

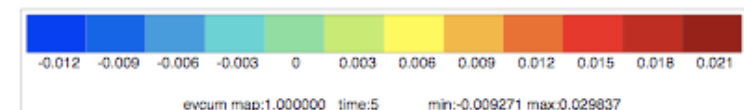
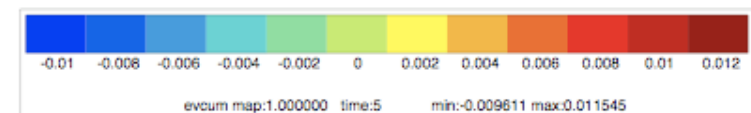
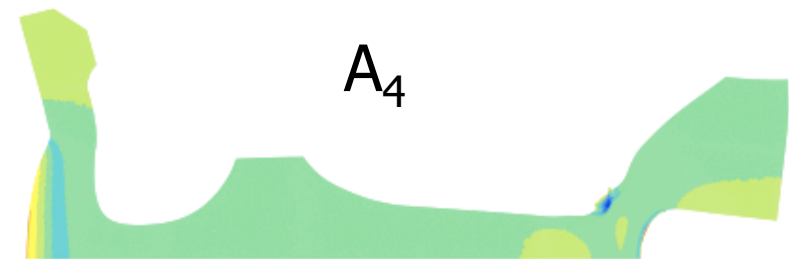
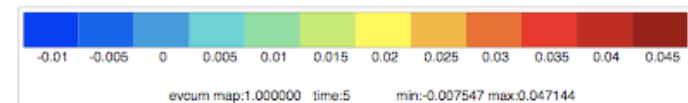
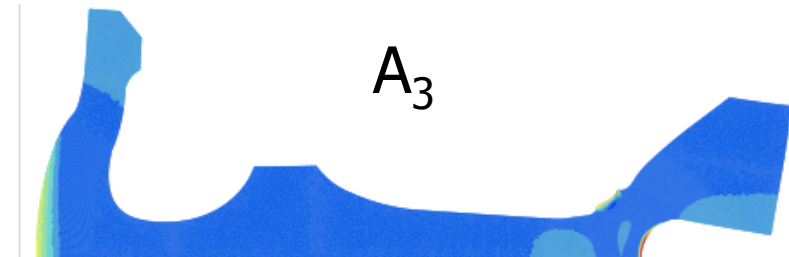
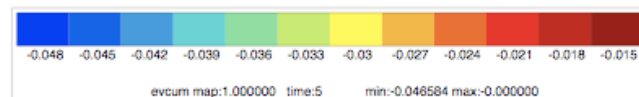
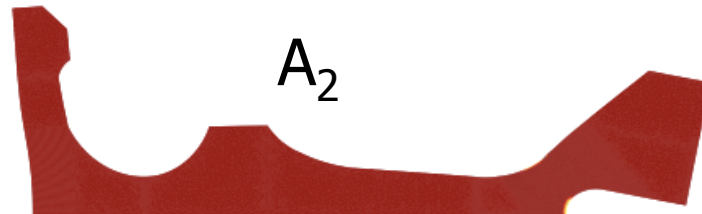
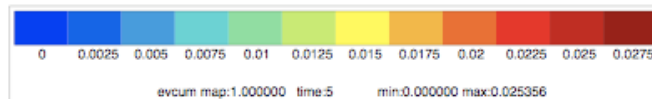
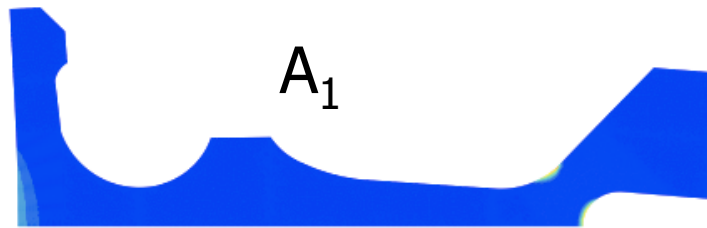


Convergence of the ROM

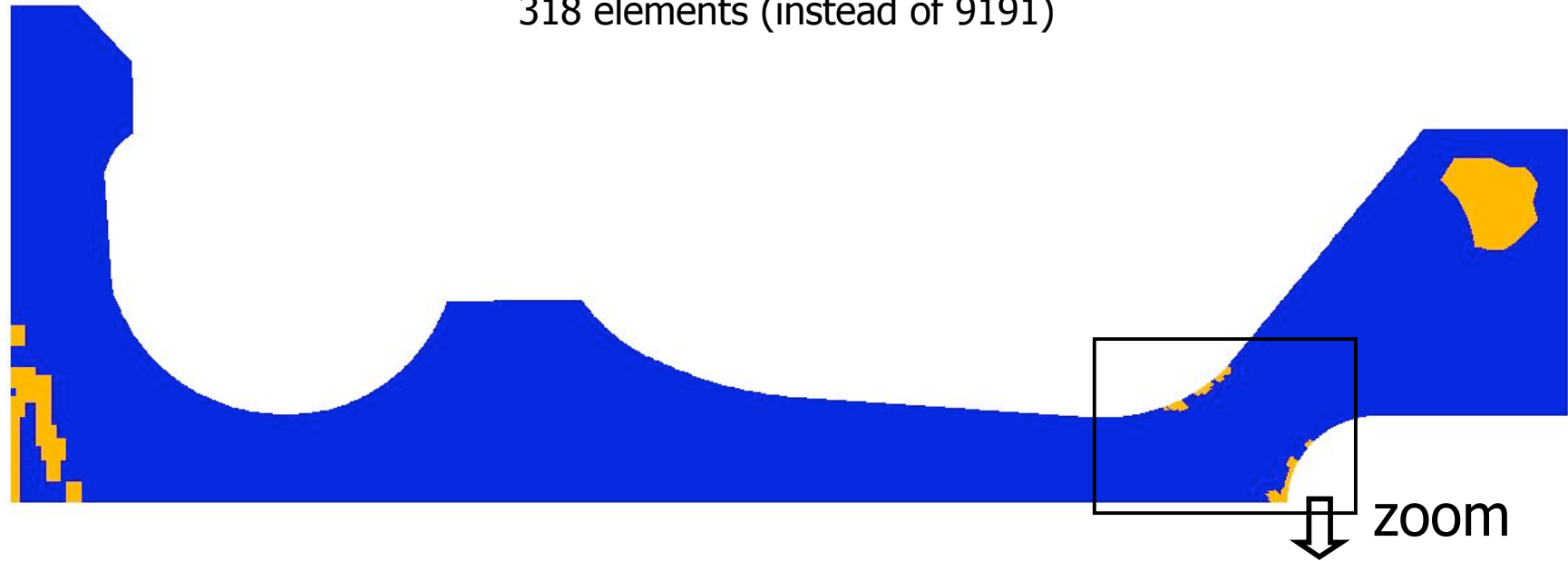


Dernière version du modèle d'ordre réduit (n = 31)

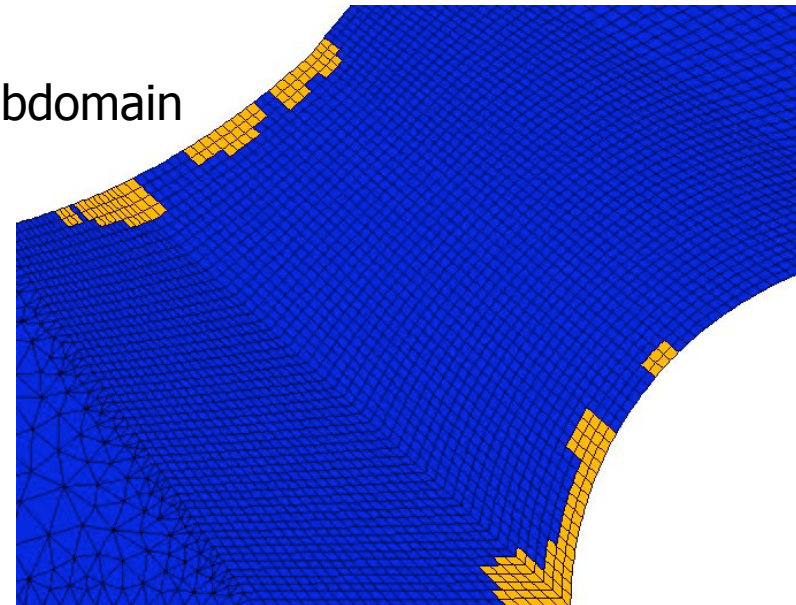
Dof : 49372 $\Rightarrow$ 5
Réduction Vint : 563941 $\Rightarrow$ 33
Elements: 9191 $\Rightarrow$ 389



The reduced integration domain
318 elements (instead of 9191)



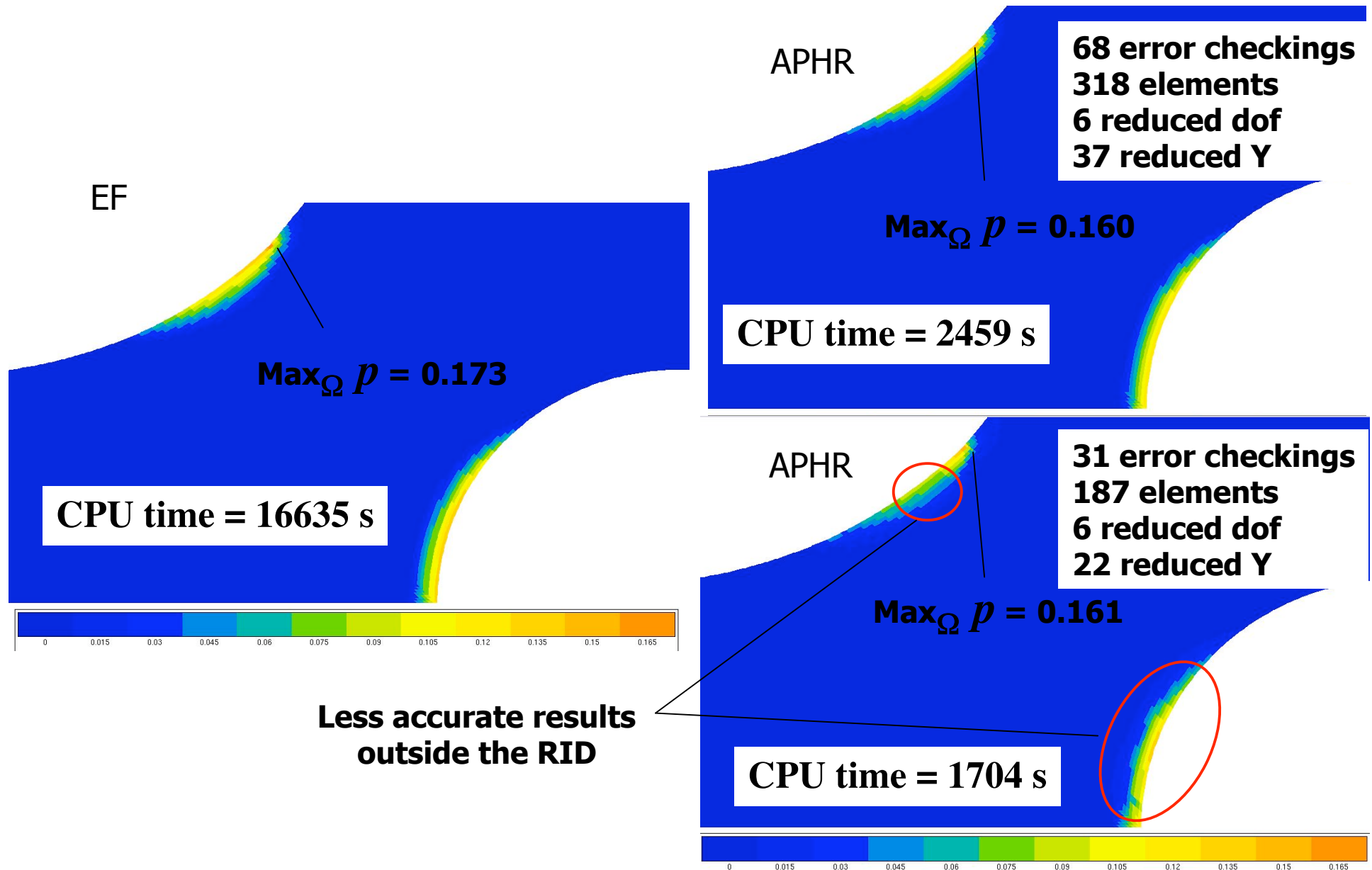
3 subdomains :
elements where $A_{Y,k}$ is maximum for each subdomain
+ elements where R_{ini} is maximum
+ connected elements



Temps CPU : FEM / APHR

FEM	APHR	Saving factor
	$\text{}^{(o)}\text{A} = \emptyset$	
Time CPU Total = 16635	Time CPU Total = 2459	6.8
Time Modified Dscpack solver = 4802	Time Modified Dscpack solver = 190	25.
Time Compute_internal_reac = 6493	Time Full FEM increments = 563	
	Time Rom adaptation = 111	
	Time Rom convergence loop = 1184	
	Time Bulding reduced integration domain = 7	
	Time initial residu for localization = 19	
Calls in Local Int = 143000000	Calls in Local Int = 12400000	
Compute_internal_reac calls = 4321	Compute_internal_reac calls = 5228	
Total Iterations = 2718	Total Iterations = 3610	

We can choose between accurate simulations or fast ones



Conclusions

Nous proposons une méthode adaptative de construction de bases réduites pour les problèmes incrémentaux.

Cette méthode construit la base POD d'une estimation de la solution du problème complet.

Une méthode d'intégration réduite a été validée pour les modèles d'ordre réduit dans le cadre de transformations thermiques et mécaniques.

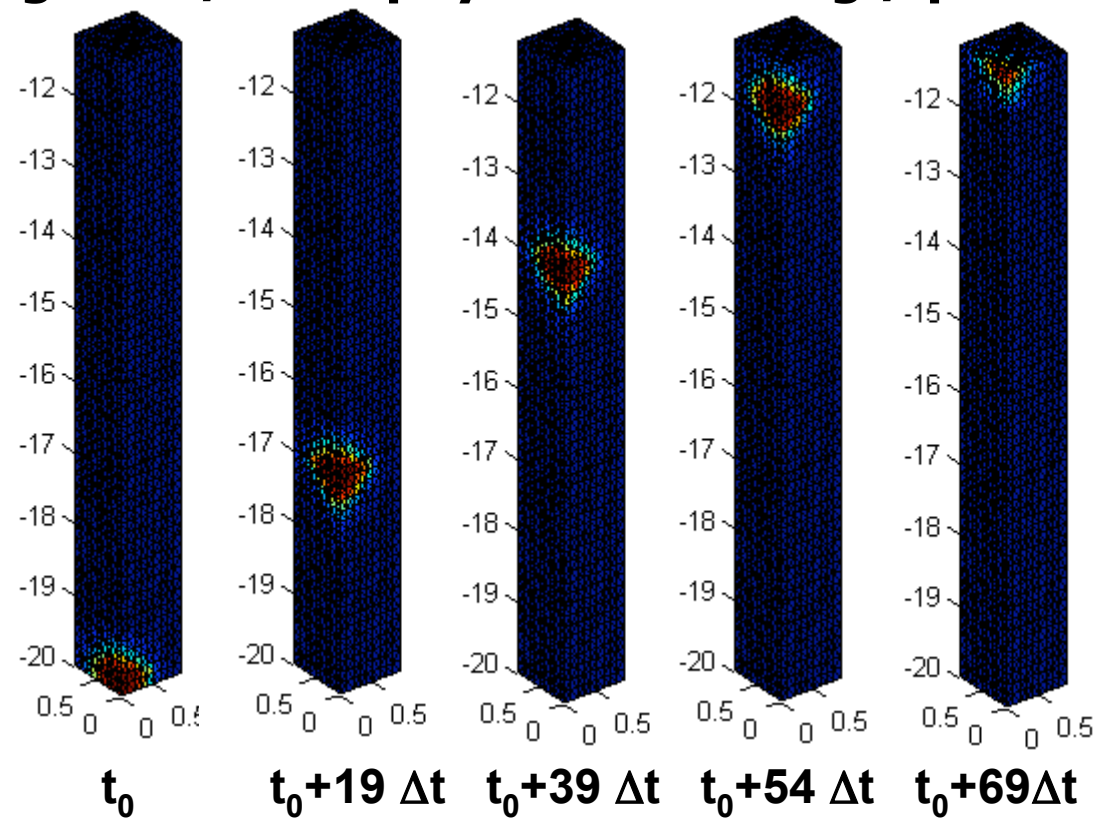
Il est possible de choisir graduellement entre des calculs à qualité maîtrisée et des calculs à durée limitée (sélection d'éléments et de fonctions de forme).

La méthode est facile à implémenter. Elle ne dépend pas du schéma d'intégration utilisé ni du type de formulation choisie.

Work in progress

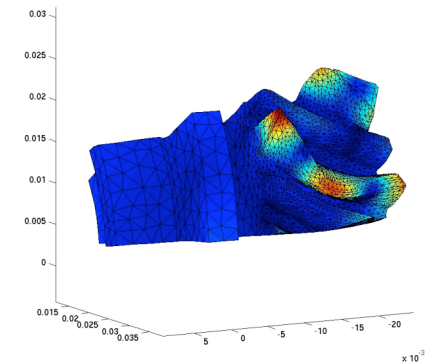
Welding simulation

Moving load / multiphysics modelling / parallel computing



Current theses related to the APHR method :

Recognition of the origin of gear distortion defaults.
L. Vanoverberghe, RENAULT

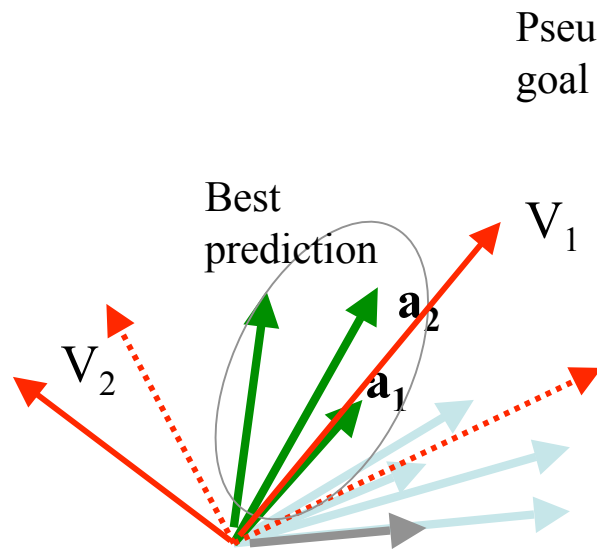


Distortion anticipation of ceramic parts.
B. Sarbandi, CRITZ3T

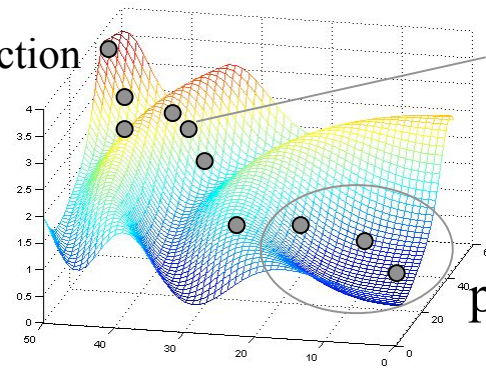
Incremental learning strategy for inverse problems.
S. Cartel, [SYSTEM@TIC](#), EHPOC

Super-element APHR.

Learning strategy



Pseudo
goal function



State evolution

The ROM must be defined on the vicinity of the best prediction.

References

On the reduction of kinetic theory models related to finitely extensible dumbbells, A. Ammar, D. Ryckelynck, F. Chinesta and R. Keunings, Journal of Non-Newtonian Fluid Mechanics, 134, pp 136-147 (2006)

On the “A Priori” Model Reduction: Overview and Recent Developments. D. Ryckelynck, F. Chinesta, E. Cueto et A. Ammar, Archives of Computational Methods in Engineering, State of the Art Reviews, Special issue, Vol. 13, n°1, pp 91-128 (2006).

An Efficient “A Priori” Model Reduction for Boundary Element Models. D. Ryckelynck, L. Hermanns, F. Chinesta et E. Alarcón, Engineering Analysis with Boundary Elements, Volume 29, Issue 8, pp 796-801, (2005).

A priori hyperreduction method : an adaptive approach, D. Ryckelynck, Journal of Computational Physics, Vol. 202 , N°1 , pp 346 - 366, (2005).

Réduction a priori de modèles thermomécaniques, D. Ryckelynck, Comptes Rendus Mécanique, Volume 330, Issue 7, Pages 499-505, (2002).